



DAAD

International Research Cooperation
PROBRAL 2007-2008 CAPES/DAAD

University of Brasília/Brazil – University of Kaiserslautern/Germany



“Networked Control with Distributed Processing
for Building Automation
in an Ambient Intelligence Framework”

Adolfo Bauchspiess

Kaiserslautern, 23.7.2006

Contents



- Brazil - Brasília – UnB
- PROBRAL
- Some on going UnB-Projects
- Energy Saving with Fuzzy Distributed Control
- Wire Less Building Automation
- Conclusions & Perspectives

BRAZIL

- Pelé - Soccer
- Carnaval - Samba
- Rio de Janeiro



Brazil

Equator

~ 8.5 Mio Km²
~ 190 Mio Inh.
~ 8.000Km Coast

BRInC

Brasília
15°45' S
47°52' W



Brasília – Capital City of Brazil

- 1960 – President J. Kubitschek, Architekt O. Niemeyer
- 1.000m over the sea level
- ~ 2 Million Inhabitants (Federal District)
- Highest income rate in south america
- Paranoá Lake



Universidade de Brasília

(Oscar Niemeyer, 1961)

1Km – Instituto Central de Ciências

FT

Technological Faculty

4 Departments

- Electrical Eng. - ~200 Beginners/Year
- Mechanical Eng.
- Civil Eng.
- Forest Eng.

6 Degrees

- Electrical Eng.
- Mechatronic Eng.
- Communication Network Eng.
- Mechanical Eng.
- Civil Eng.
- Forest Eng.



Electrical Engineering Department

43+ lecturers in 5 areas:

Control and Automation, Telecom, Electronics,
Power Systems & Communication Networks.

Areas organized in research groups,

GRAV – Grupo de Robótica, Automação e Visão Computacional

LAVSI – Laboratório de Automação, Visão e Sistemas Inteligentes

LARA – Laboratório de Robótica e Automação

GRAV

Associate Prof. Dr. Adolfo Bauchspiess

Adjoint Prof. Dr. Geovany de Araújo Borges

Adjoint Prof. Dr. João Yoshiyuki Ishihara

Adjoint Prof. Dr. Marco A. F. Egito Coelho



PROBRAL

PROgrama de Cooperação Internacional BRasil-ALEmanha

“Networked Control with Distributed Processing
for Building Automation
in an Ambient Intelligence Framework”

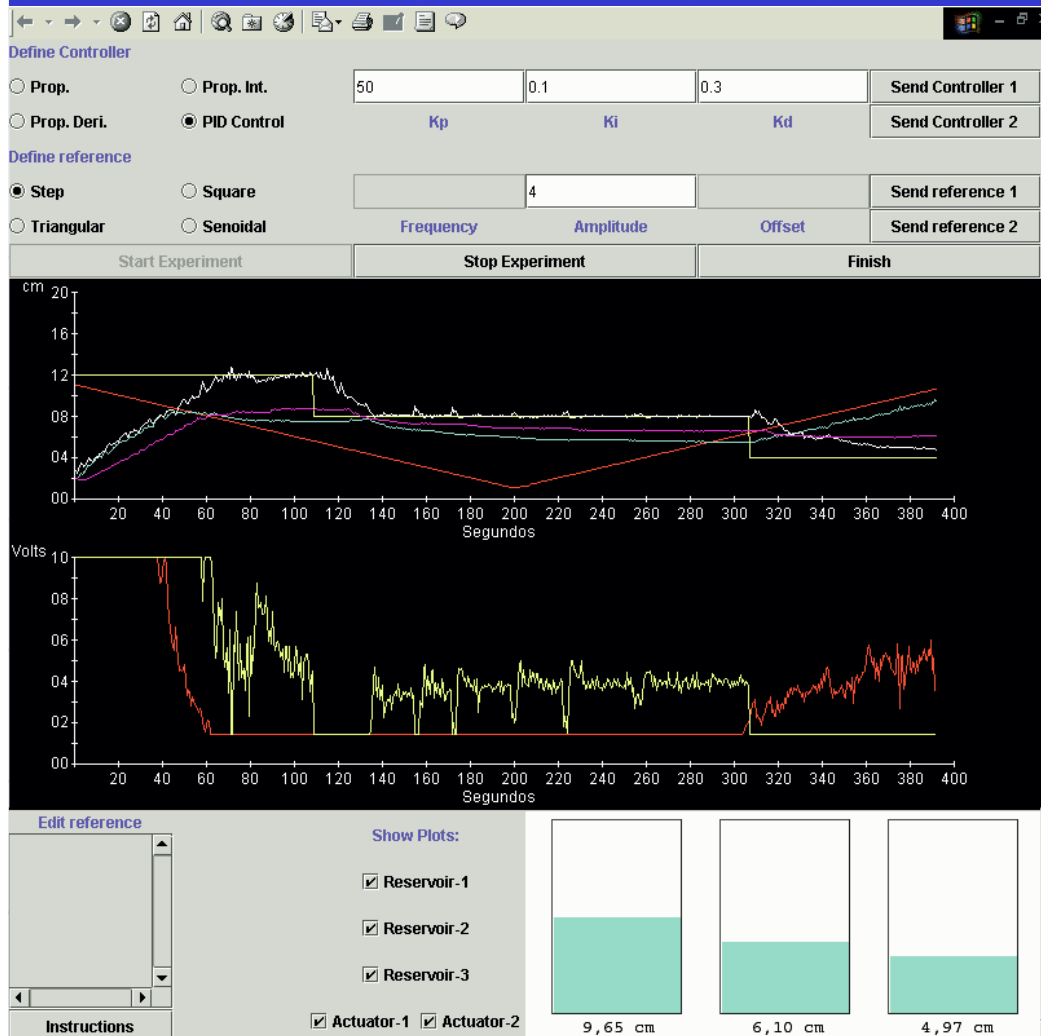
- Only supports Interchange of Researchers
- Each side must have local research (\$) support
- ~ 2 Profs. + 2 Ph.D candidates / Year
- 2 (+ 1) Years

Some on-going UnB-Projects

- LEARn
- Expansion-CARCARAH
- ...
- Related with PROBRAL:
 - SAPIEn
 - CT-Energ
 - FINEP-INOVA

LEARn

Laboratório de Ensino de Automação Remota.



UAV Inspection of Power Transmission Lines

Project Carcarah
-Expansion Ltda
-ANEEL



Projects: SAPIEn, CT-Energ and FINEP-INOVA

Energy-Saving Approach:

Model-Based HVAC Control

$$J = \underbrace{\sum_{i=1}^{h_p} (y(k+i) - y_R)^2}_{\text{comfort related}} + \underbrace{\sum_{i=0}^{h_c-1} \Delta \mathbf{u}^T(k+i) \mathbf{Q}_{\Delta u} \Delta \mathbf{u}(k+i) + \mathbf{u}^T(k+i) \mathbf{Q}_u \mathbf{u}(k+i)}_{\text{energy related}}$$

Where :

h_p – prediction horizon

h_c – control horizon

y – controlled variable

y_R – reference

u – manipulated variable

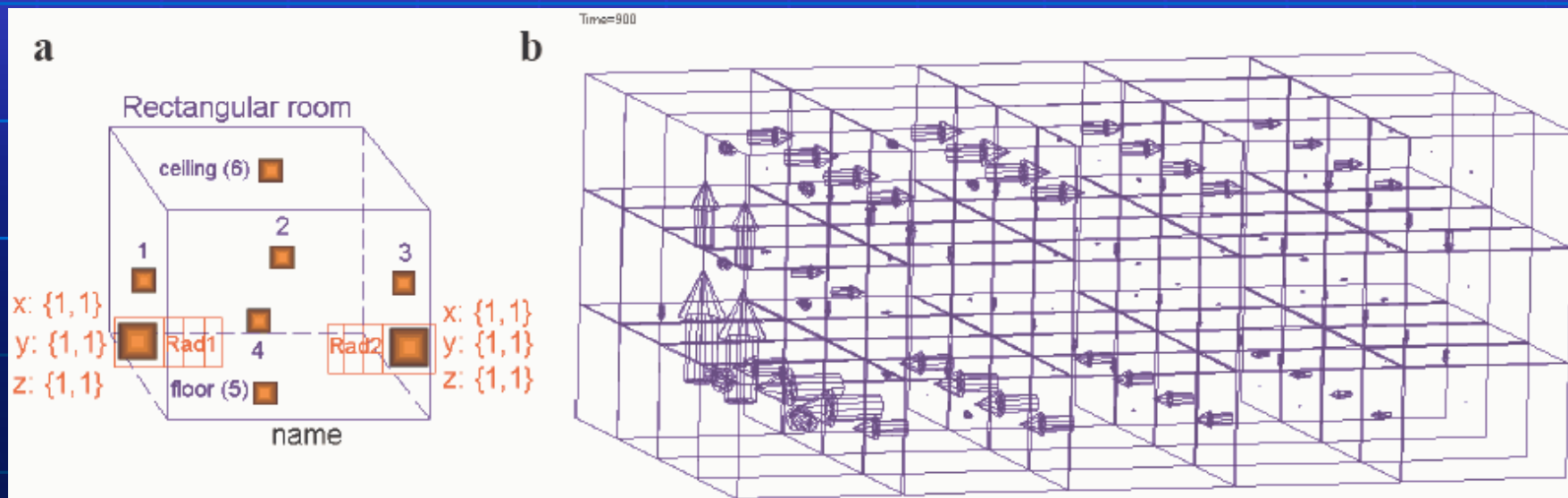
$\mathbf{Q}_{\Delta u}, \mathbf{Q}_u$ – weighting matrices

Predictive Cost Function:

Considers comfort and energy saving. Needs model!

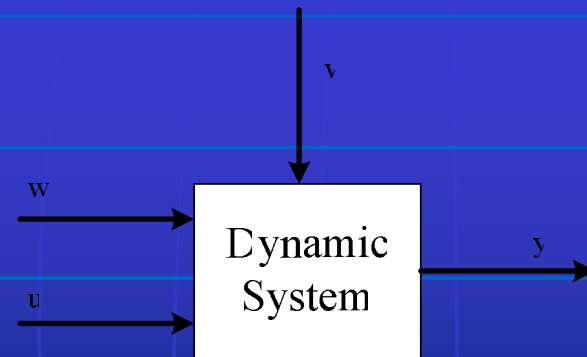
Distributed Parameter Modelling

- Transport Phenomena
- Ex. Heat Flow



Wind velocity simulation in Modelica, by Felgner, ASIM2002

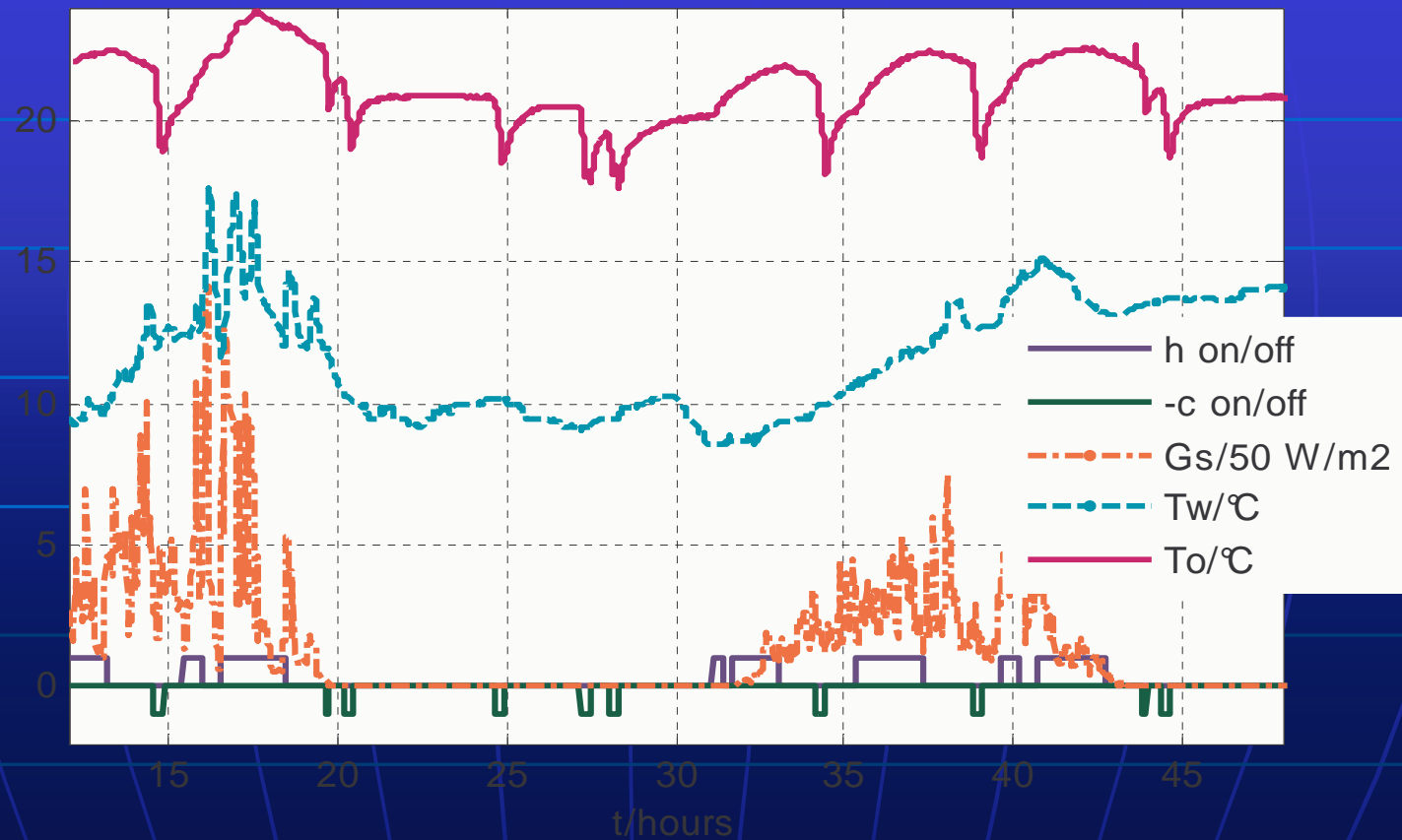
Dynamic System Identification



u – input (manipulated variable)
 y – output (controlled variable)
 w – measurable disturbance
 v – non-measurable disturbance

First-Principles Identification (KL-2006)

Identification data set of March 29-31, 2006



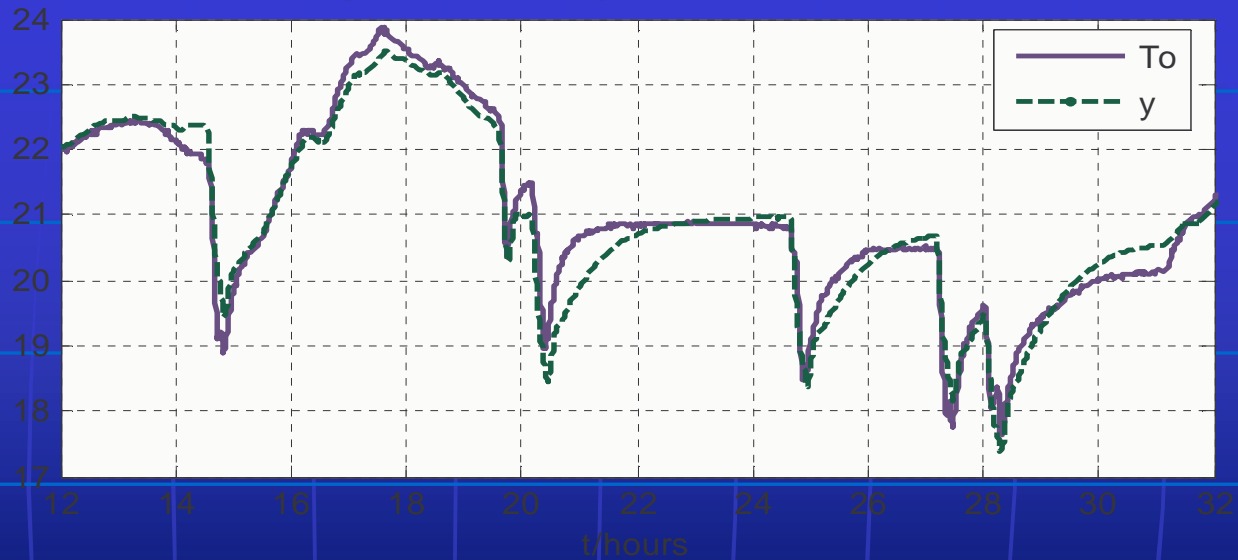
Typical identification data set

a) Linear MISO approach

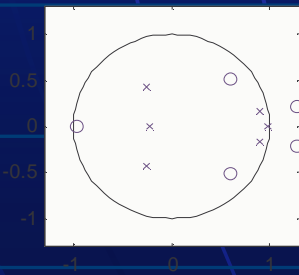
$u=[T_h \ T_c \ T_w \ T_v \ G_s]$ 6th order MISO model

$$\dot{x} = Ax + Bu + Ee$$

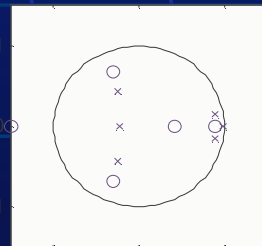
$$y = Cx + Du$$



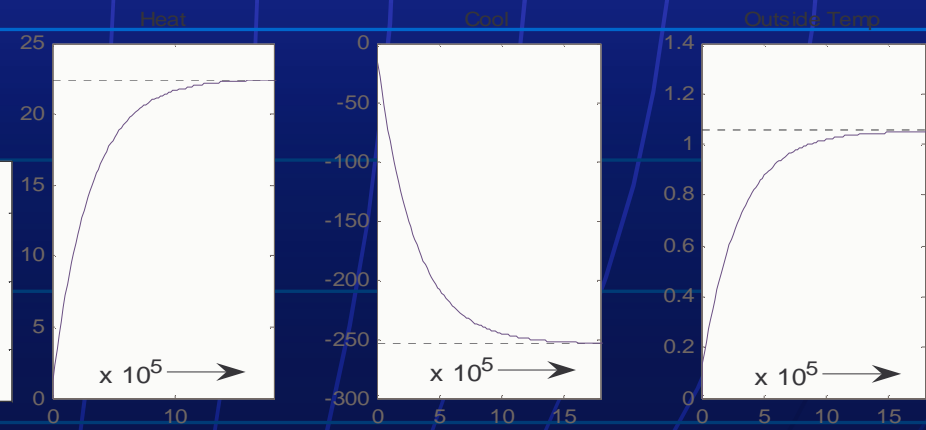
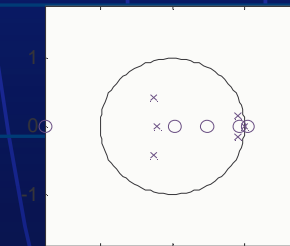
From T_h



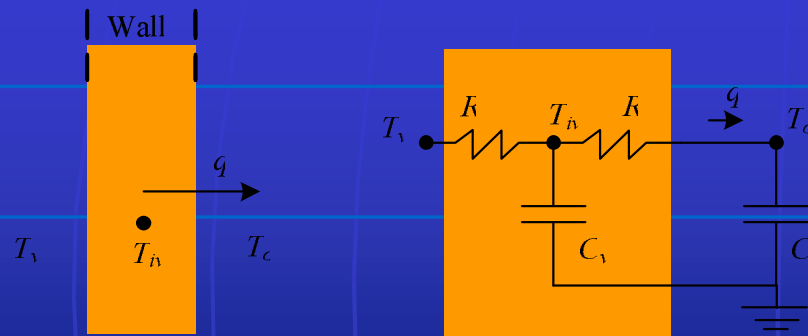
From T_c



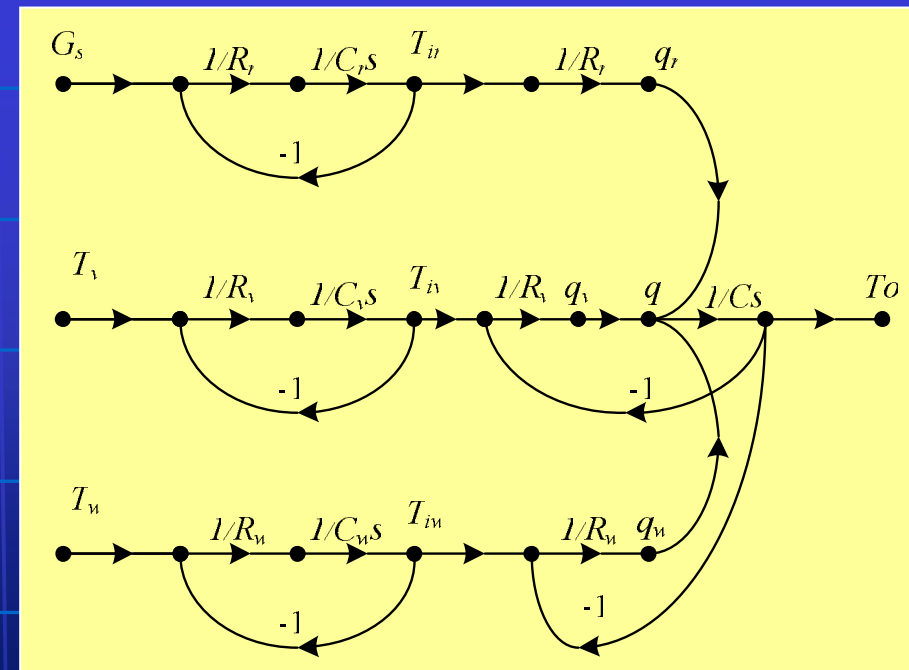
From T_w



b) First-Principles Structured Identification



2R1C analogy of the vicinity heat transfer

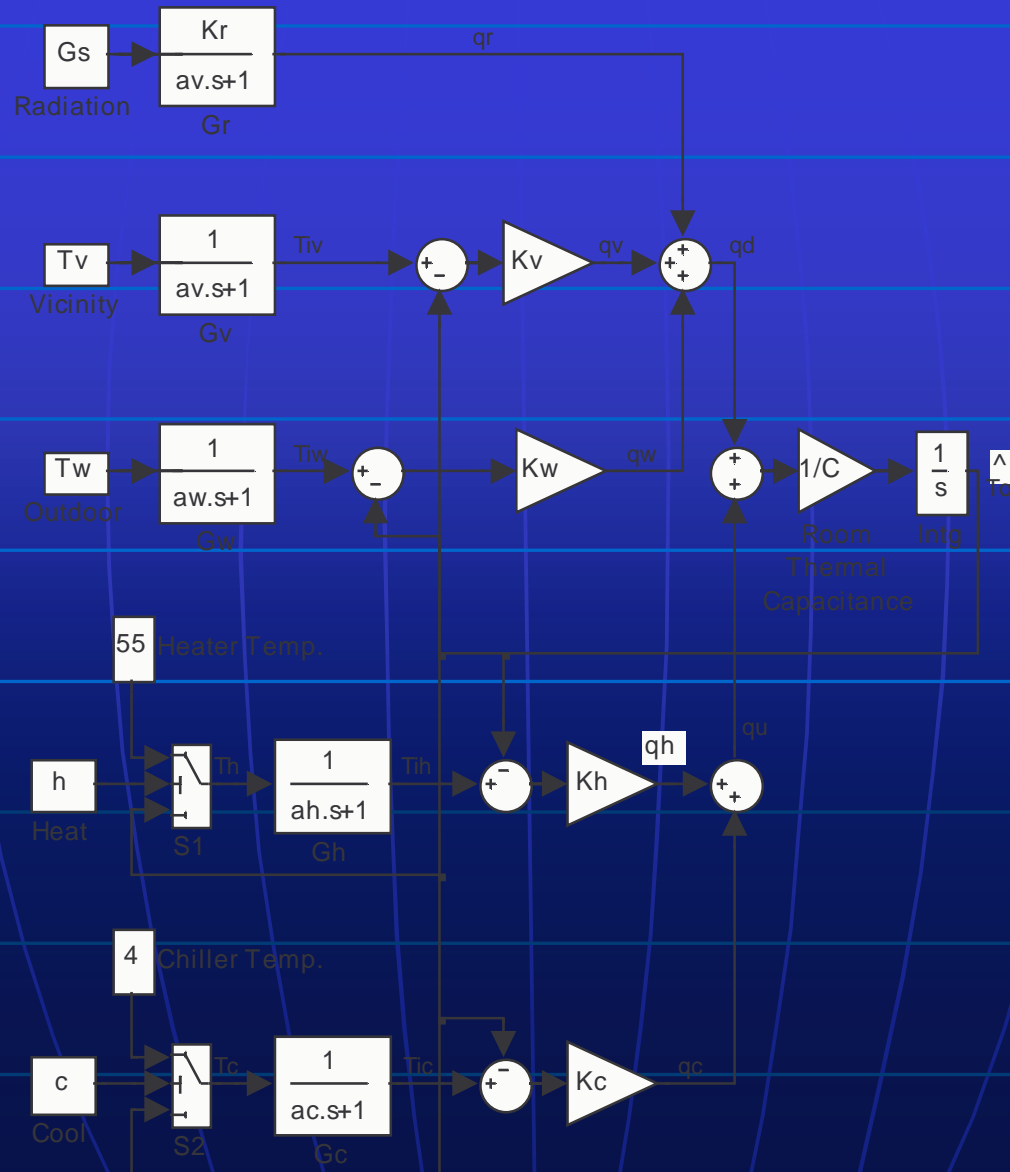


2R1C-based disturbance model

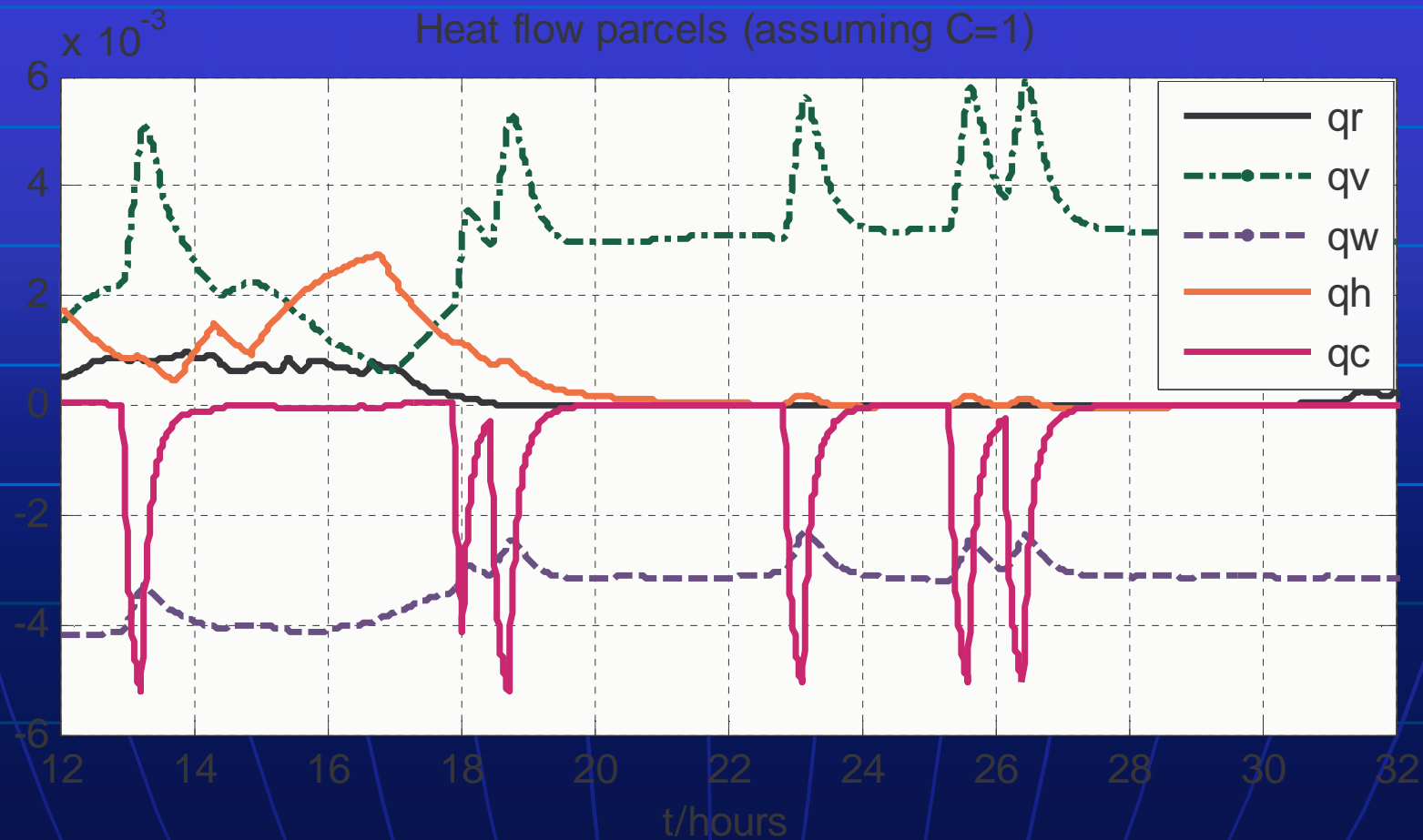
Heat flow due to disturbances:

$$q_d = \frac{aK_r s G_s(s)}{(as+1)(a_r s+1)} + \frac{aK_v s T_v(s)}{(as+1)(a_v s+1)} + \frac{aK_w s T_w(s)}{(as+1)(a_w s+1)}$$

First-principles structured thermal model

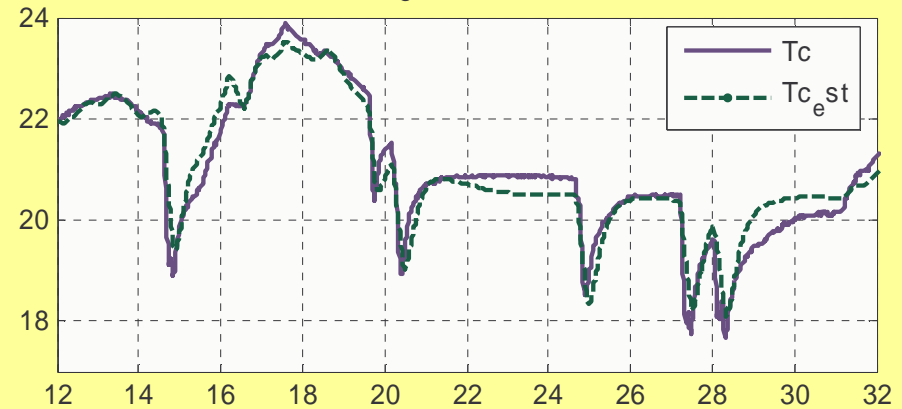


Heat flow obtained with the first-principles structured identification

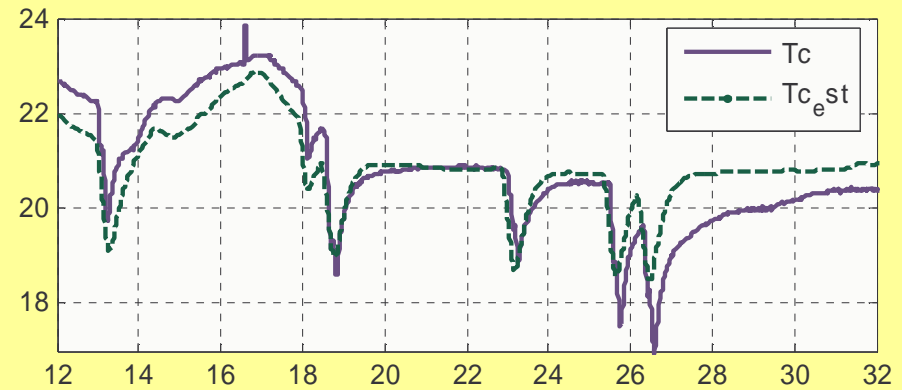


Results of the first-principles structured identification

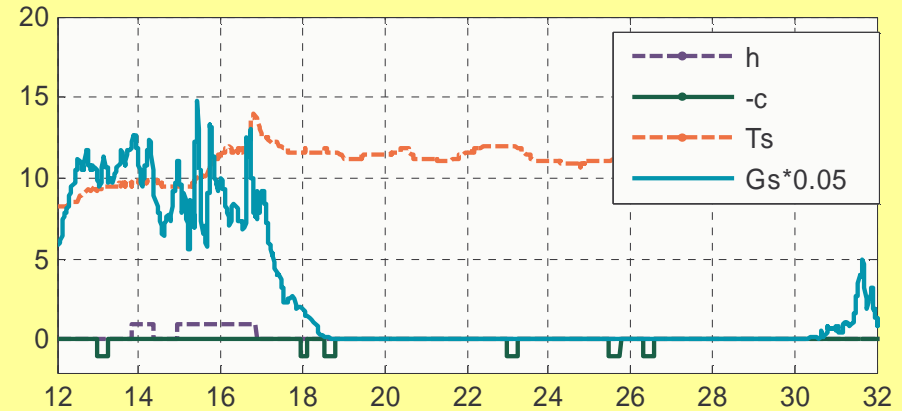
Results - Training data - March 29-31, 2006



$T_c/^\circ\text{C} - T_{c_est}/^\circ\text{C}$ - Validation - March 24-27, 2006



Heat, Cool, Weather and Solar Radiation - March 24-27, 2006



PROBRAL-Related

SAPIEn –

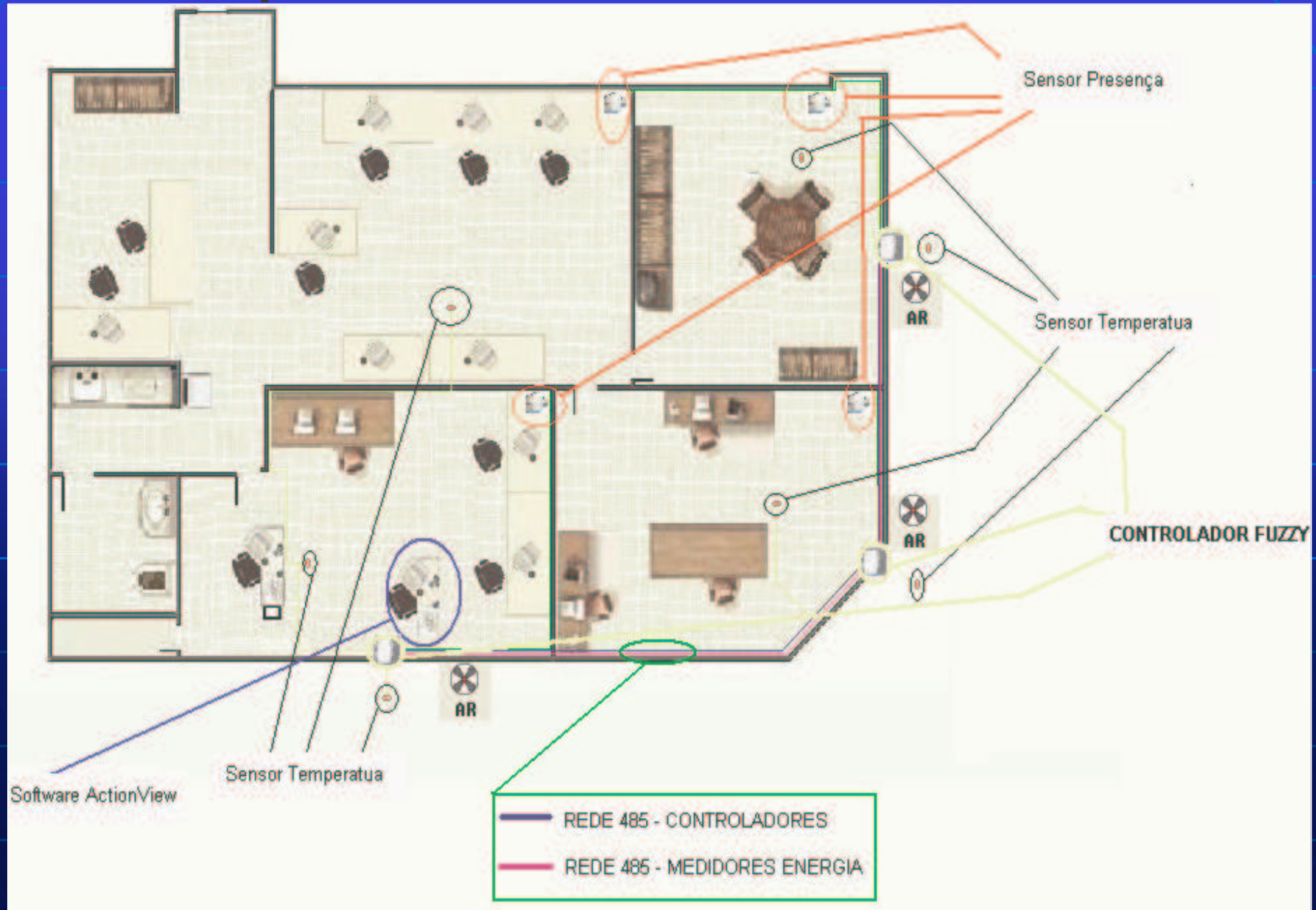
Energy Saving by Fuzzy Distributed Control

- Energy Saving
- Thermal Comfort
- Building Automation
- FAP-DF suport



Campus UnB (2007) 995 window air conditioners
>R\$1.000.000,00/Year (1€ ≈ 2,56 R\$)

Experimental Environment



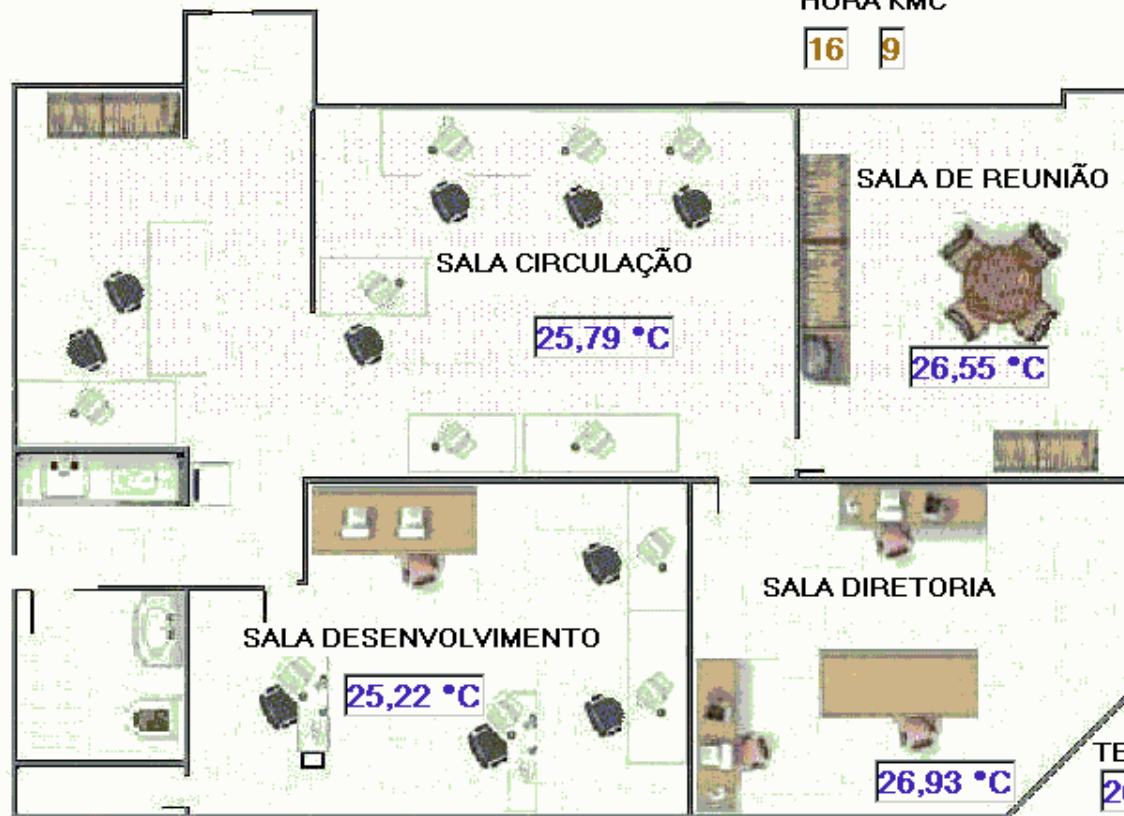


SUPER



HORA KMC

16 9



TEMPERATURA EXTERNA
26,55 °C

TEMPERATURA EXTERNA
26,55 °C

SETPOINT
24,50 °C

TEMPERATURA EXTERNA
32,46 °C

ActionView - Run Time - [Alarmes Correntes Número de Linhas=3]

Apresentar Ação Editar Exportar Imprimir Configuração Janela Acessórios Ajuda

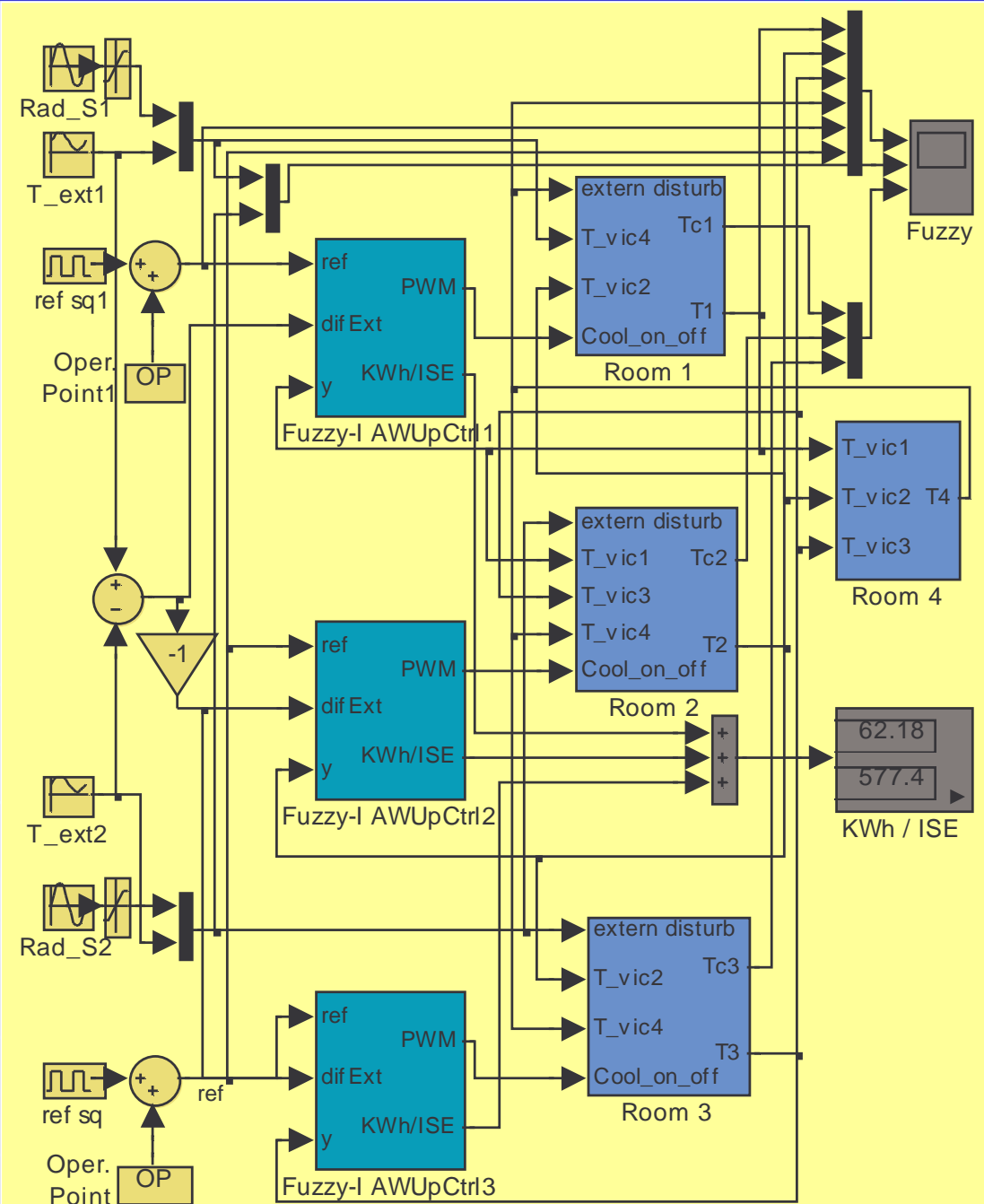
R	Rec	Data	Hora	Sistema	Grupo	Tipo	Descrição	Grandeza	Valor	Limite
R	<input checked="" type="checkbox"/>	19/09/2006	15:09:41,000	SPN	AR_1	MAX EMERG	AR_1 TEMPERATURA EXTERNA	Temperatura	32,12	32 °C
R	<input checked="" type="checkbox"/>	19/09/2006	15:10:11,000	SPN	AR_2	MAX EMERG	AR_2 TEMPERATURA EXTERNA	Temperatura	32,09	32 °C
R	<input checked="" type="checkbox"/>	19/09/2006	15:09:50,000	SPN	AR_3	MAX EMERG	AR_3 TEMPERATURA EXTERNA	Temperatura	32,46	32 °C

SIMULATION

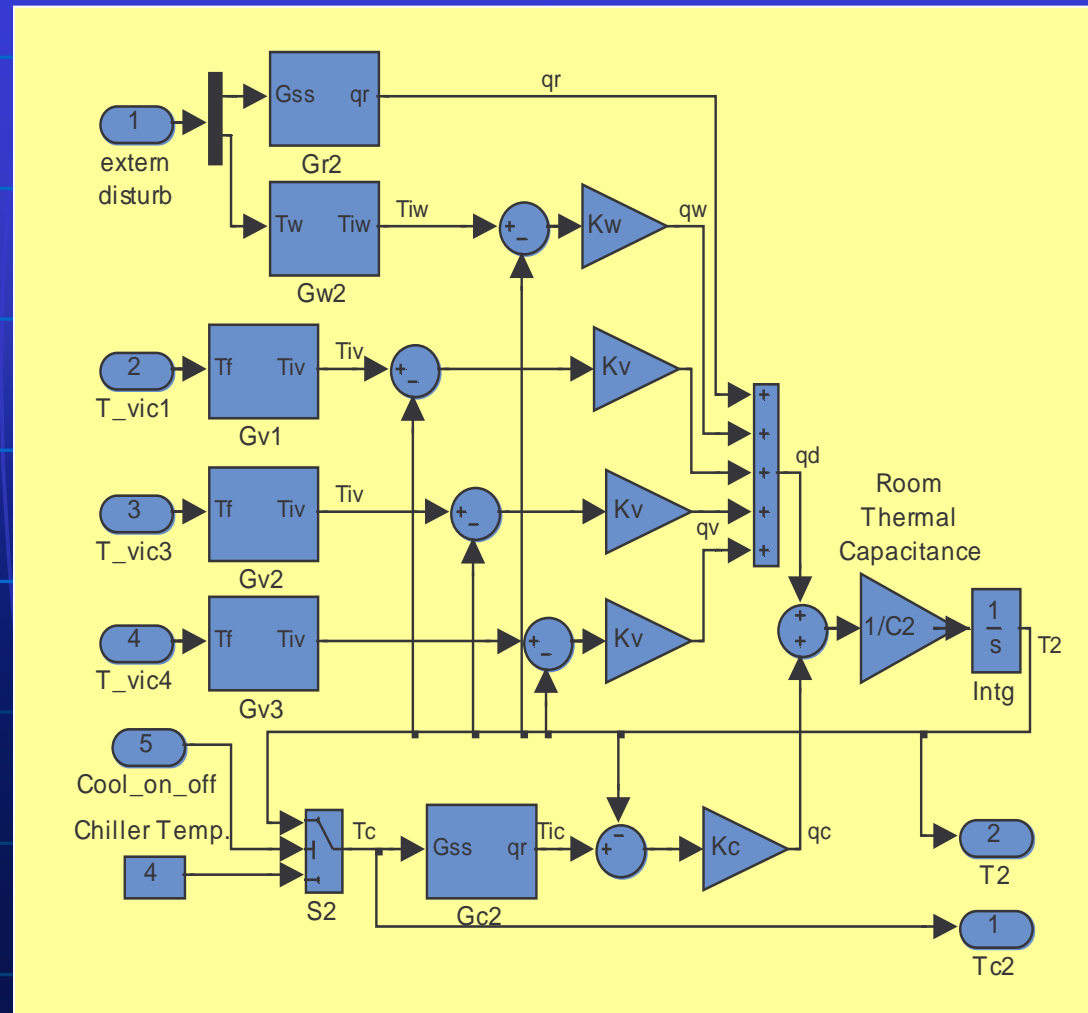
Simulink®

MIMO process:

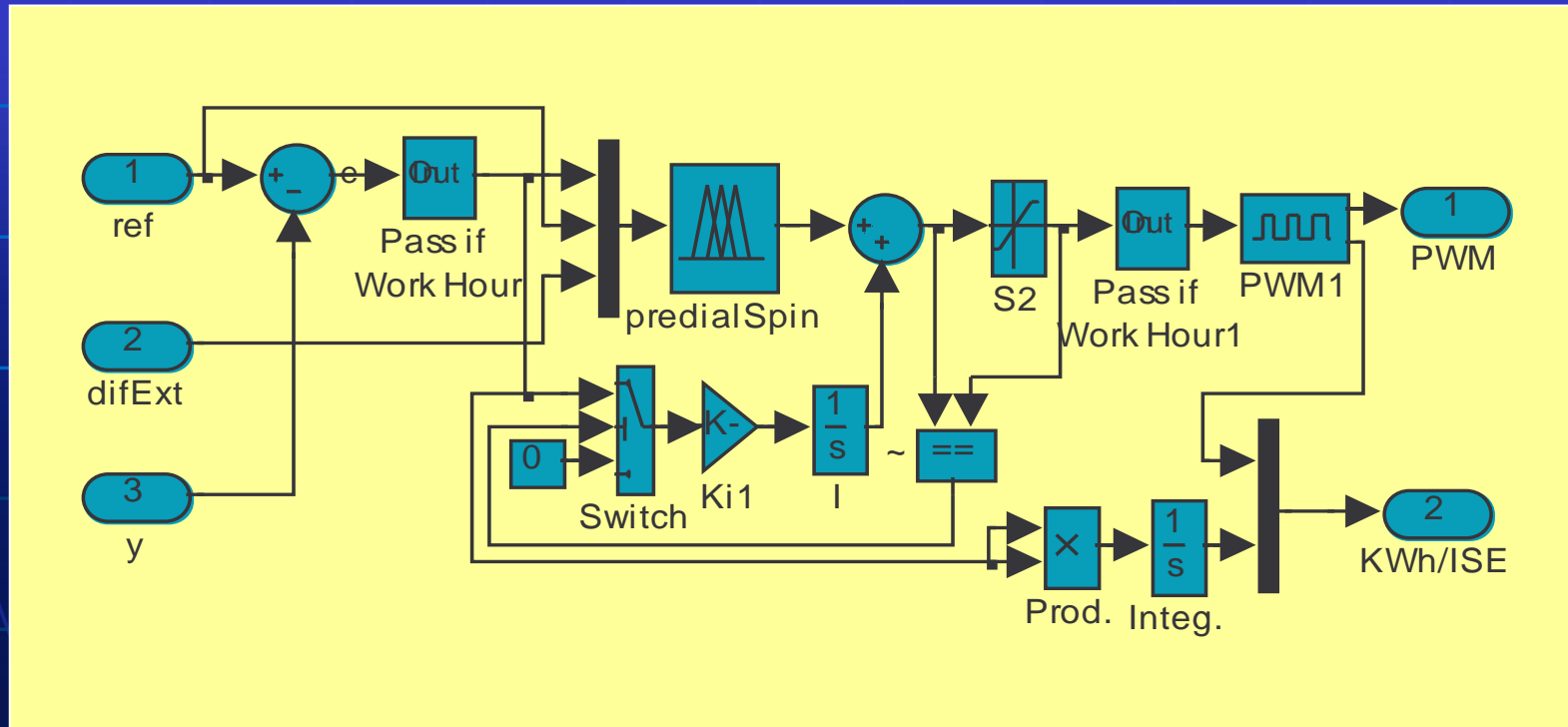
- 4 rooms
- 3 air conditioners



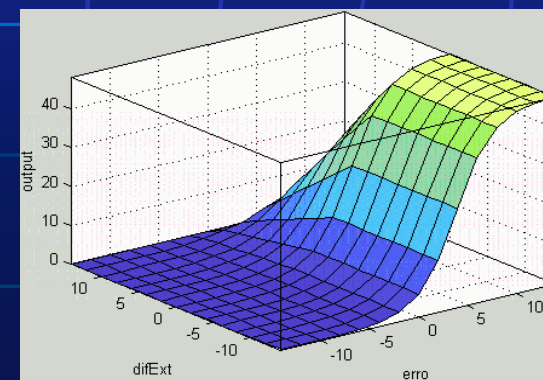
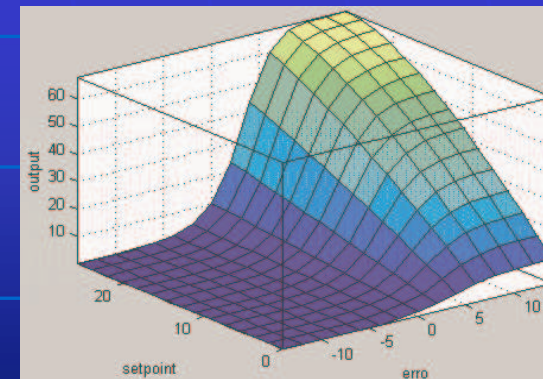
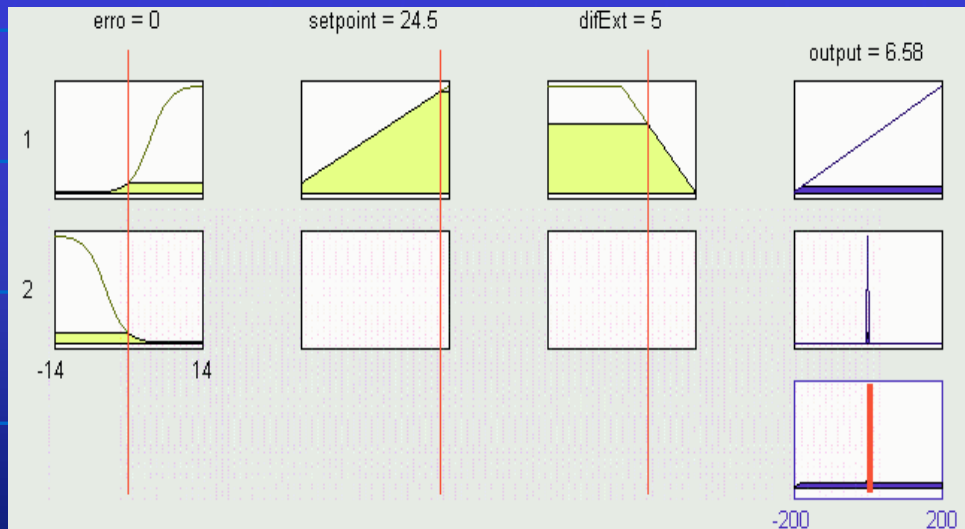
Room Model



Controller

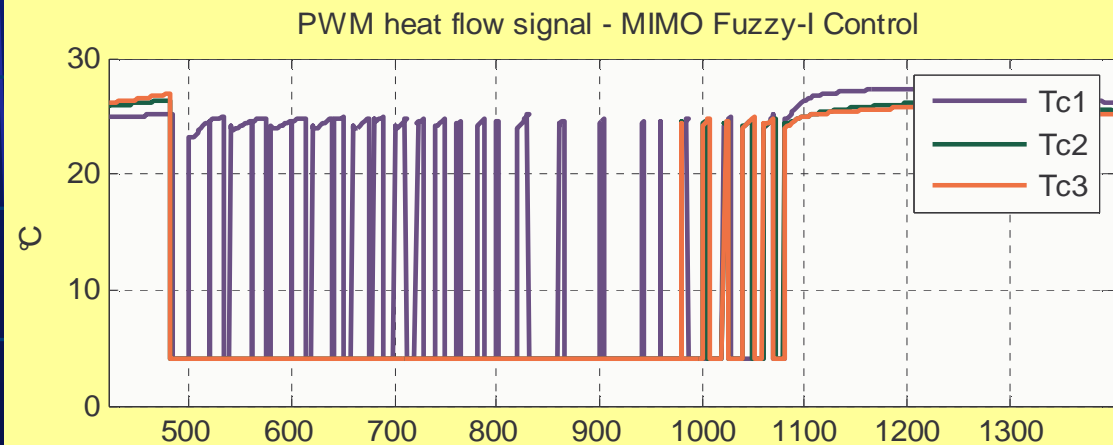
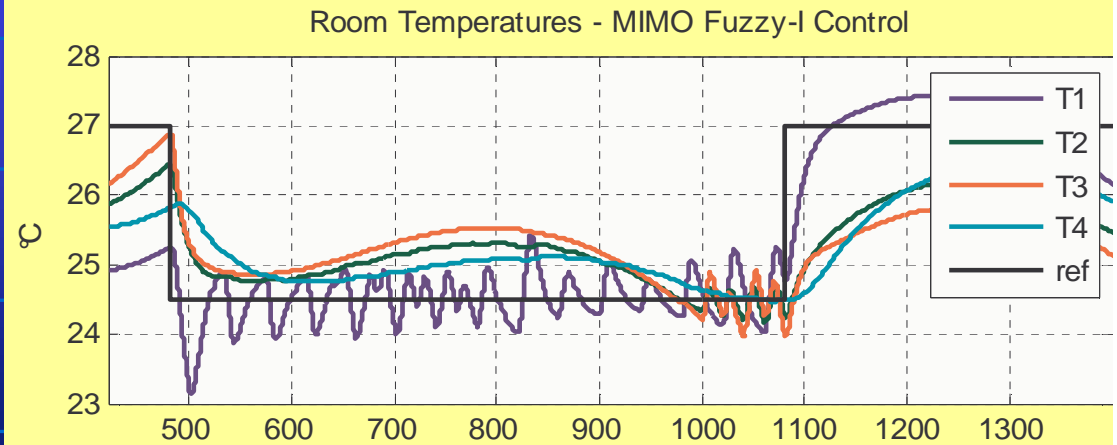
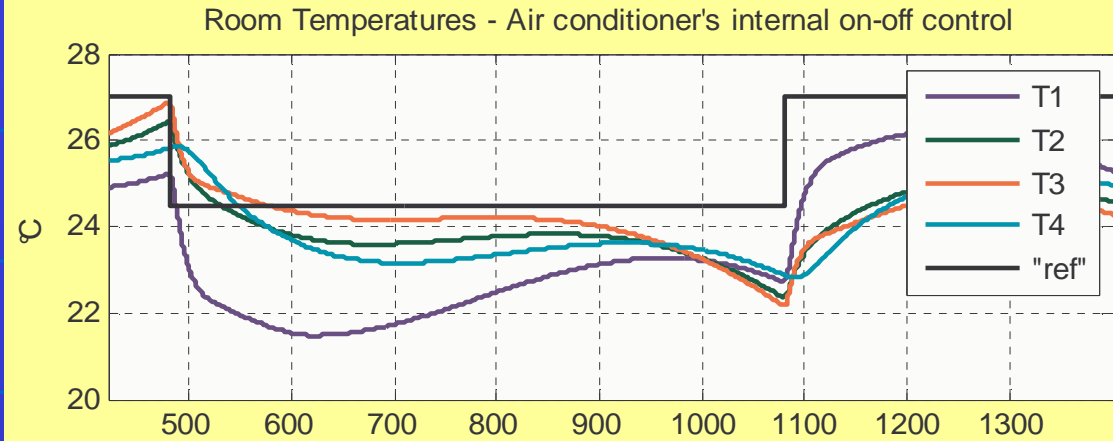


Fuzzy Rule Basis



- 1) IF (erro = p) AND (setpoint = set) AND (Difext = d) THEN (output = p)
- 2) IF (erro = n) THEN (output = zero)

Simulation Results



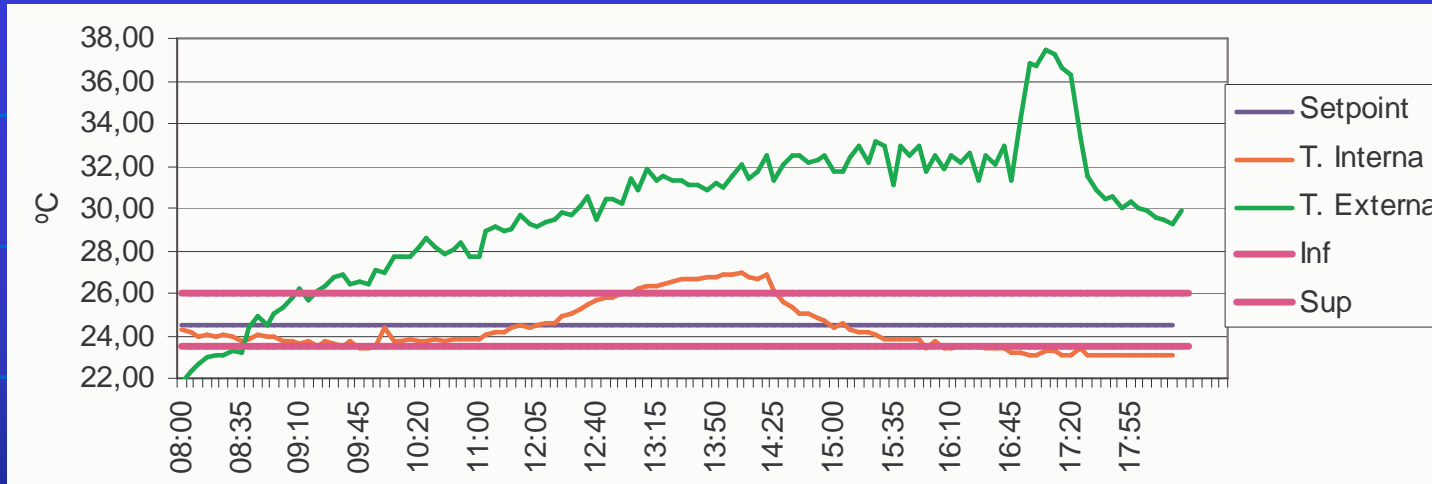
Distributed building controller Prototype

Programmable Logic Controller
KMC 7000 (~R\$300,-)

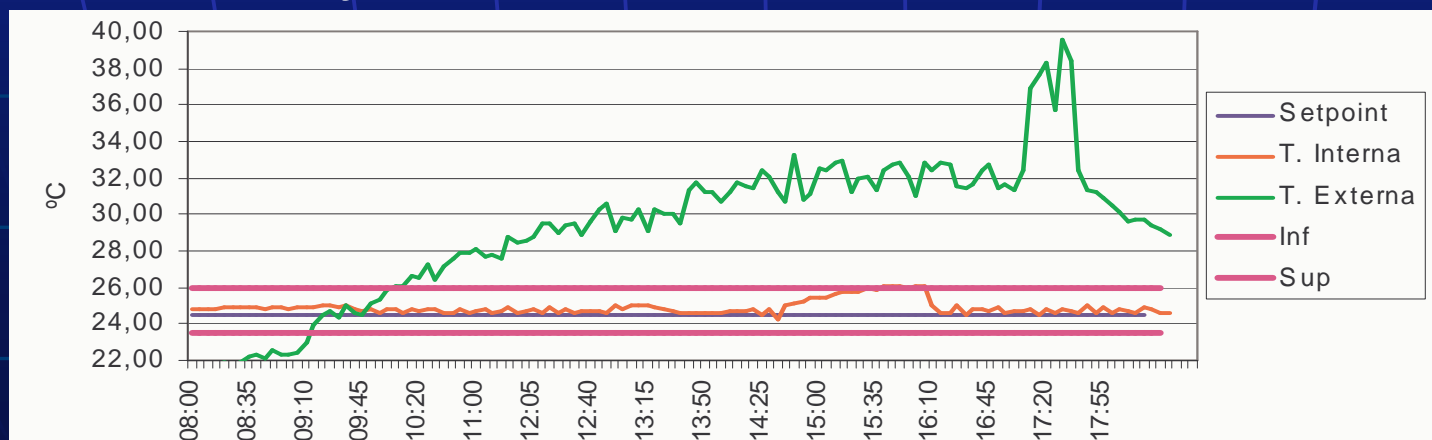


Developing Room

On-Off 16-09-2006

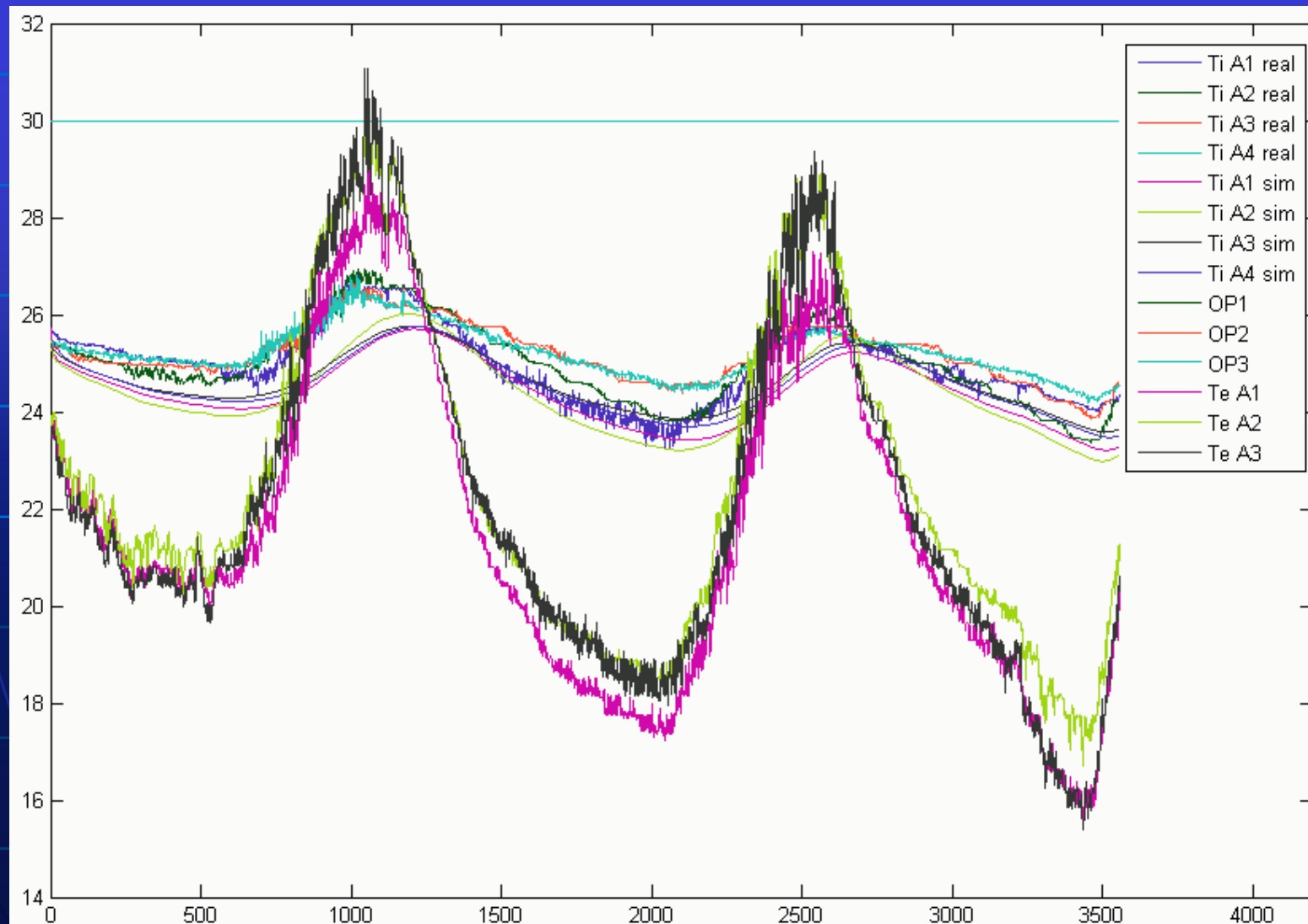


Fuzzy Control 14-09-2006



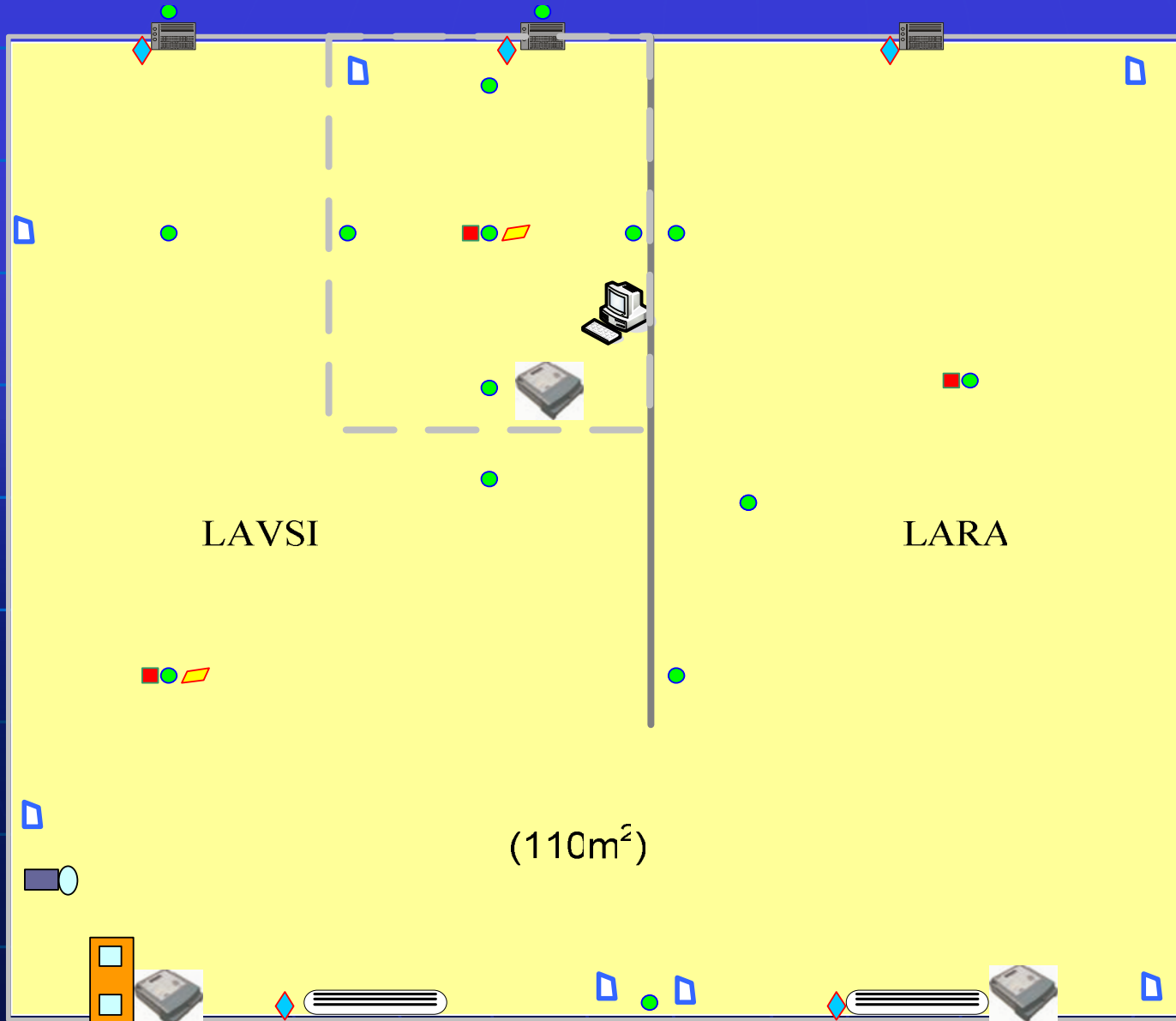
~30% saving!












Measured and Reconstructed Signals - Multi-Room Experiment (June 2007)



Intelligent Building Automation

Wire Less Prototype – LAVSI-LARA/ENE-UnB



-  Air Cond Actuator
-  Temperature Sensor
-  Humidity Sensor
-  Anemometer
-  Presence Sensor
-  Access Control (Finger Print)
-  USB Camera Infra-Red
-  Air Cond
-  Split Air Conc
-  Energy Meter 3Φ
-  BAS - Building Automation System

Singular Systems (Descriptor Systems)

João Yoshiyuki Ishihara

Outline

- Introduction
- What is a singular system (descriptor system)?
- Examples of descriptor modeling
- Some results: stability, filtering
- Future work related to PROBRAL

What is a singular system (descriptor)?

$$f(x(t), \dot{x}(t), u(t)) = 0$$

Implicit equations

Linear case

$$E\dot{x}(t) = Ax(t) + Bu(t)$$

Singular equations

In particular:

$$\dot{x}(t) = Ax(t) + Bu(t)$$

Usual state-space equations

What is a singular system (descriptor)?

Another characterization

$$E\dot{x}(t) = Ax(t) + Bu(t)$$

Can be re-written as:

$$\begin{aligned}\dot{x}(t) &= Fx(t) + Gu(t) \\ 0 &= Hx(t) + Ju(t)\end{aligned}$$

Differential-algebraic equations

Descriptor model

RLC circuit equations

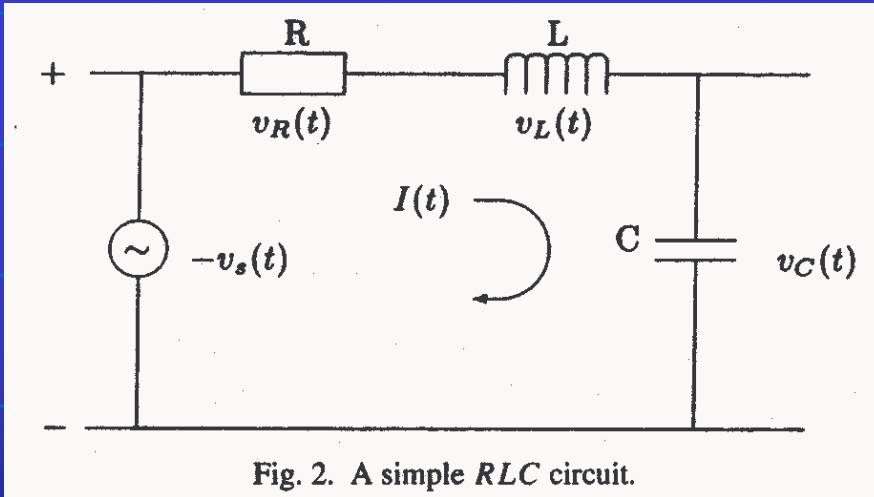


Fig. 2. A simple RLC circuit.

$$L \frac{dI(t)}{dt} = v_L(t)$$

$$\frac{dv_C(t)}{dt} = \frac{1}{C} I(t)$$

$$0 = -RI(t) + v_R(t)$$

$$0 = v_L(t) + v_C(t) + v_R(t) + v_S(t)$$

$$E\dot{x}(t) = Ax(t) + Bu(t)$$

$$\begin{bmatrix} L & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \dot{I}(t) \\ \dot{v}_L(t) \\ \dot{v}_C(t) \\ \dot{v}_R(t) \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 1/C & 0 & 0 & 0 \\ -R & 0 & 0 & 1 \\ 0 & 1 & 1 & 1 \end{bmatrix} \begin{bmatrix} I(t) \\ v_L(t) \\ v_C(t) \\ v_R(t) \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \end{bmatrix} v_S(t)$$

descriptor equations

$$y(t) = [0 \ 0 \ 1 \ 0]x(t)$$

Example: Robot with Restricted Motion



Minimização de energia para robôs com restrição
Trabalho de mestrado no LAC - Aluno: Cauê Peres
Orientador: Paulo Sérgio P. da Silva

Apr. 2007

Robot with Restricted Motion

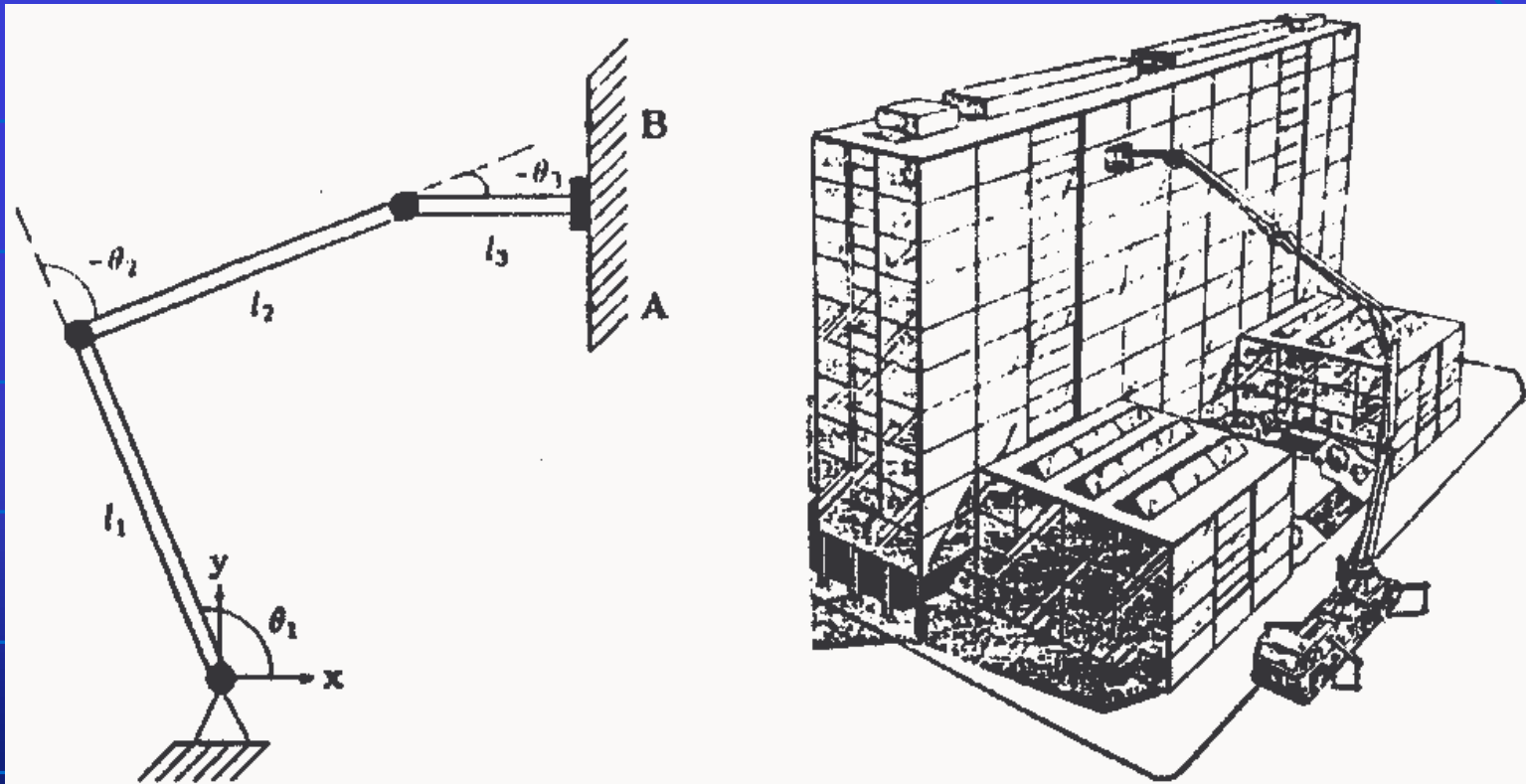


Fig. 1. A three link mobile manipulator [29].

$$\begin{bmatrix} I_3 & 0 & 0 \\ 0 & M_0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \dot{x} = \begin{bmatrix} 0 & I_3 & 0 \\ -K_0 & -D_0 & F_0^T \\ F_0 & 0 & 0 \end{bmatrix} x + \begin{bmatrix} 0 \\ S_0 \\ 0 \end{bmatrix} u$$

Example: Perturbation analysis of large systems

Large systems: small parameters are set to zero

$$\begin{aligned}x_1(k+1) &= A_{11}x_1(k) + A_{12}x_2(k) + B_1u(k) \\ \epsilon x_2(k+1) &= A_{21}x_1(k) + A_{22}x_2(k) + B_2u(k)\end{aligned}$$

Simplified model

$$\begin{aligned}x_1(k+1) &= A_{11}x_1(k) + A_{12}x_2(k) + B_1u(k) \\ 0 &= A_{21}x_1(k) + A_{22}x_2(k) + B_2u(k)\end{aligned}$$

$$Ex(k+1) = Ax(k) + Bu(k)$$

Example: interconnected systems

Large systems: collection of interconnected subsystems

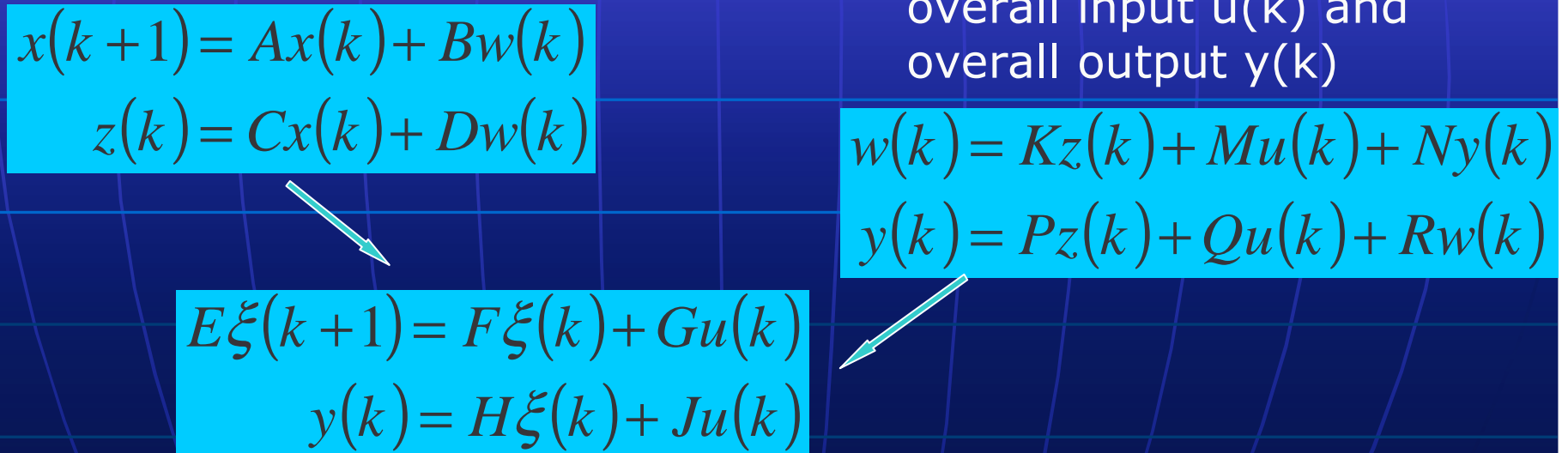
$$\begin{aligned}x_i(k+1) &= A_i x_i(k) + B_i w_i(k) \\ z_i(k) &= C_i x_i(k) + D_i w_i(k)\end{aligned}$$

Overall subsystem equation

$$\begin{aligned}x(k+1) &= Ax(k) + Bw(k) \\ z(k) &= Cx(k) + Dw(k)\end{aligned}$$

Interconnections:
overall input $u(k)$ and
overall output $y(k)$

$$\begin{aligned}w(k) &= Kz(k) + Mu(k) + Ny(k) \\ y(k) &= Pz(k) + Qu(k) + Rw(k)\end{aligned}$$


$$\begin{aligned}E\xi(k+1) &= F\xi(k) + Gu(k) \\ y(k) &= H\xi(k) + Ju(k)\end{aligned}$$

Obs: A state-space representation may not exist
for some interconnected systems

A system with no state equations

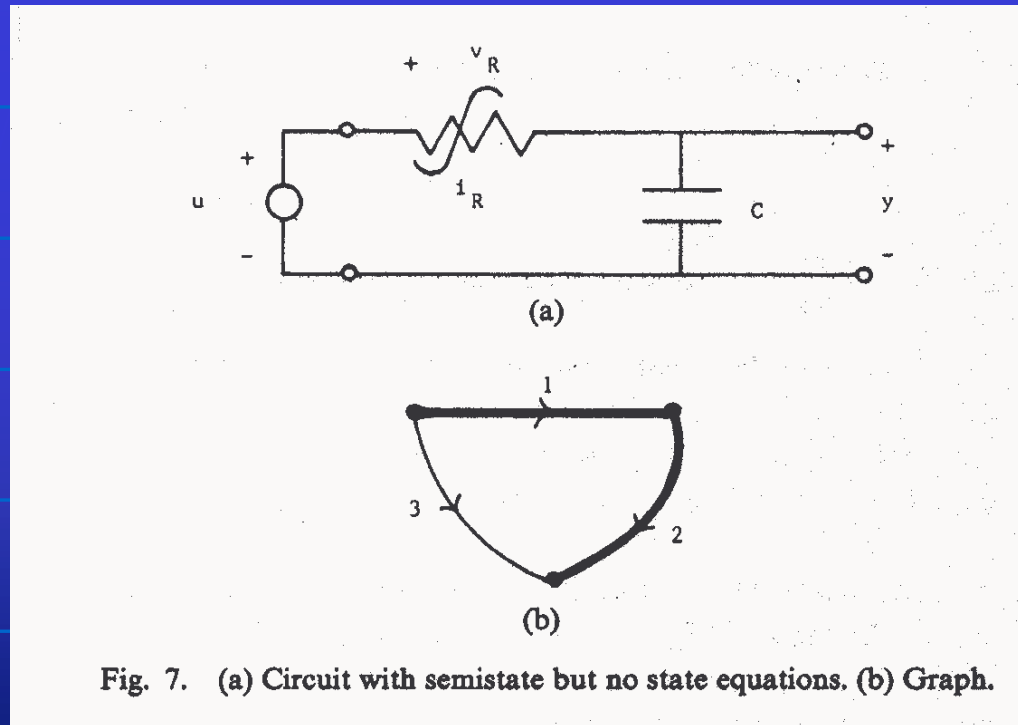


Fig. 7. (a) Circuit with semistate but no state equations. (b) Graph.

$$v_R = -3i_R + i_R^3$$

$$\begin{bmatrix} 0 & C & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \dot{x} + \left\{ \begin{bmatrix} 0 & 0 & 1 \\ 1 & 1 & 0 \\ 1 & 0 & -3 \end{bmatrix} x + \begin{bmatrix} 0 \\ 0 \\ x^3 \end{bmatrix} \right\} = \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix} u$$

$$y = [0 \quad 1 \quad 0]x$$

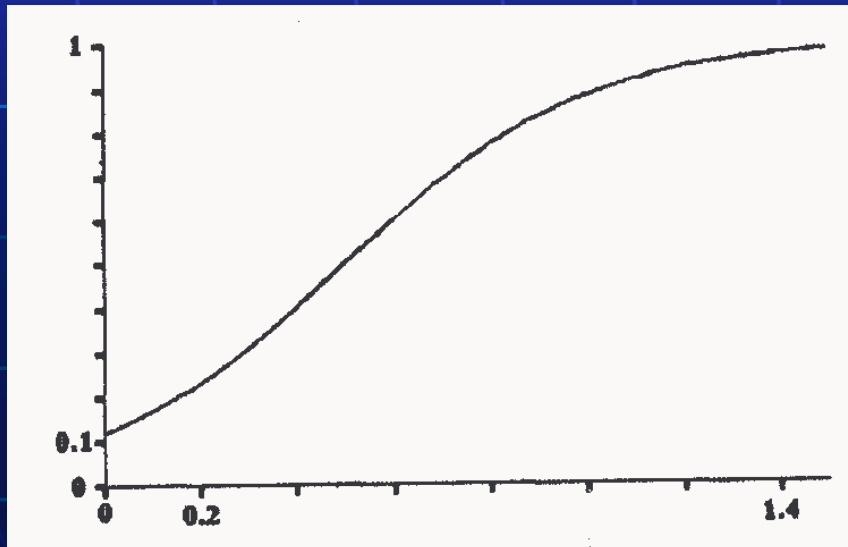
Example 2: system with no state equations

Agricultural production growing curve

$$\dot{\bar{y}}(t)/\bar{y}(t) = \kappa(\bar{y}^* - \bar{y}(t))$$

Logistic function

$$\bar{y}(t) = \bar{y}^* \frac{e^{\kappa \bar{y}^* (t-t^*)}}{1 + e^{\kappa \bar{y}^* (t-t^*)}}$$



3 parts:

- * Exponential growth
- * Linear growth
- * Logarithmic growth

Example 2: system with no state equations

The agricultural production growing curve is solution of the following singular system

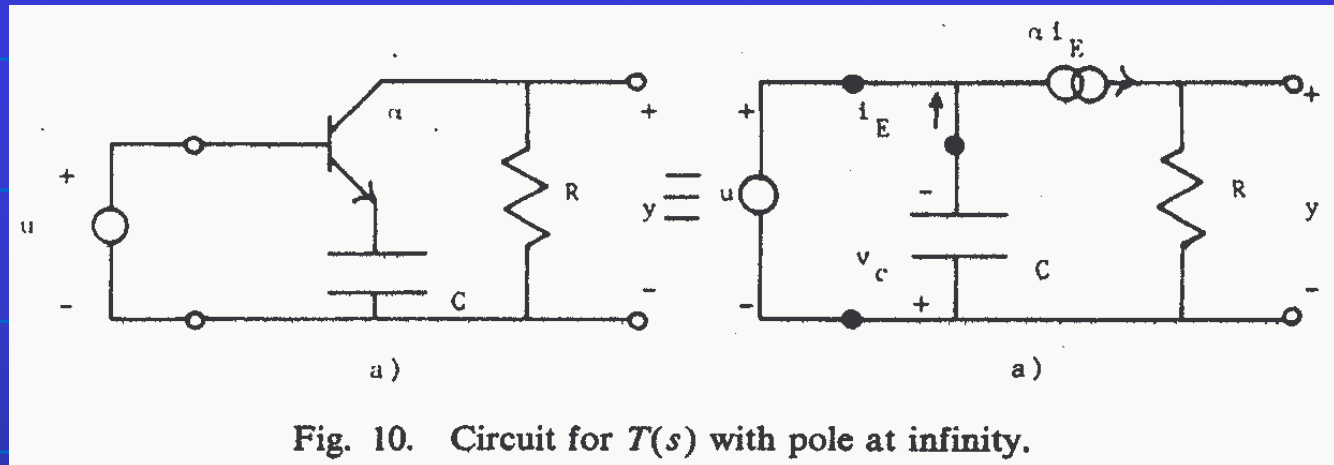
$$\begin{bmatrix}
 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\
 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\
 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\
 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\
 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1
 \end{bmatrix} \dot{x} = \begin{bmatrix}
 -\bar{s}_1 & -s_1 \\
 a-1 & 0 \\
 0 & 0 \\
 0 & 0 \\
 0 & 0
 \end{bmatrix}$$

$$+ \begin{bmatrix}
 \frac{1}{|\alpha|} - \alpha & 1 & \alpha & \alpha & 0 & 0 & 0 & 0 \\
 -\bar{a} & -a & 1 - a\alpha & 1 & 0 & 0 & 0 & 0 \\
 \alpha - 1 & 0 & -\alpha & -\alpha & \frac{1}{|s_2|} & 1 & 0 & 0 \\
 0 & 0 & -1 & 0 & \frac{1}{|s_2|} - 1 & 0 & 1 & 0 \\
 0 & 0 & 0 & 0 & s_2 - 1 & -s_2 & 0 & 0
 \end{bmatrix} x$$

$$+ \begin{bmatrix}
 0 & 0 & 0 & 0 & (\omega_0^2 \cdot |\alpha| \cdot |a|) \\
 |a|^{-1} & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0
 \end{bmatrix}^T u$$

$$y = \begin{bmatrix}
 0 & 0 & 0 & 0 & (\omega_0^2 \cdot |\alpha| \cdot |a|) \\
 |a|^{-1} & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0
 \end{bmatrix} x$$

Impulsive Responses



Transistor model

$$\begin{bmatrix} C & 0 \\ 0 & 0 \end{bmatrix} \dot{x}(t) = \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix} x(t) + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u(t), \quad t \geq 0, \quad x = \begin{bmatrix} v_C \\ i_E \end{bmatrix}$$

$$y = [0 \quad \alpha R] x$$

In the state space formulation we have information loss
(Impulsive solution)

Example: Filtering of non causal system

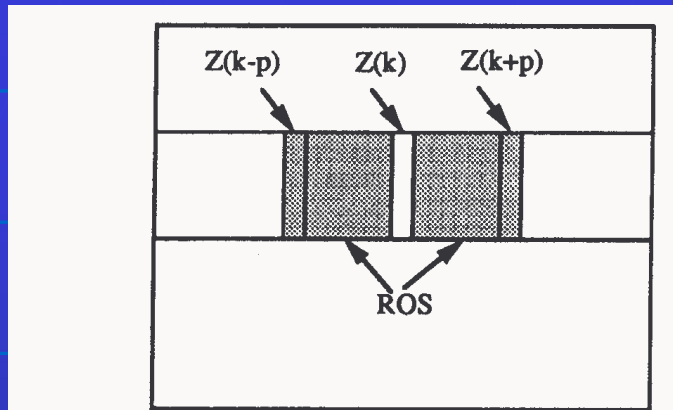


Fig. 1. ROS of noncausal model.

$$Ex(k+1) = Fx(k) + Gu(k)$$

$$z(k) = Hx(k)$$

$$x(k) = \left[z^T(k-p) \quad z^T(k) \quad z^T(k+p) \right]^T$$

$$E = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}, \quad F = \begin{bmatrix} 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \\ \frac{\rho}{1+\rho^2} & 0 & -1 & 0 & \frac{\rho}{1+\rho^2} & 0 \\ 0 & \frac{\rho}{1+\rho^2} & 0 & -1 & 0 & \frac{\rho}{1+\rho^2} \end{bmatrix}$$

$$G = \begin{bmatrix} 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}^T$$

$$H = \begin{bmatrix} 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \end{bmatrix}$$

Pros and Cons for descriptor modeling

- Riccati equations are related to Hamiltonian extended pencils (which are in descriptor form)
- State-space systems are not closed under PID feedback
- Any rational transfer function can be represented by a descriptor system

Pros and Cons for descriptor modeling

- It is a very natural way to model process dynamics.
- It refers much more to the physical behavior of the system and gives more physical insight.
- The interpretation of results is also more simple than in case of the more abstract state space models.

Application: Liquid Level Control System

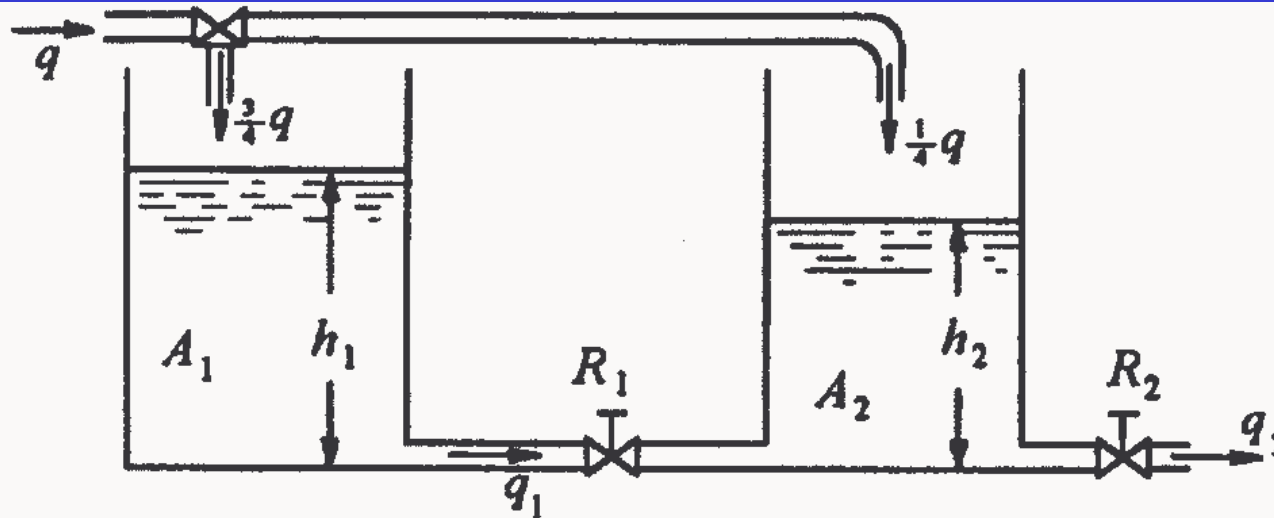


Figure 1: A liquid-level control system

q, q_1, q_2 : rates of the flow of liquid (m^3/sec);

A_1, A_2 : areas of the cross-section of tanks (m^2);

h_1, h_2 : liquid levels (m);

R_1, R_2 : flow resistance (sec/m^2);

Application: Liquid Level Control System

State Space Model

$$\begin{bmatrix} \dot{h}_1 \\ \dot{h}_2 \end{bmatrix} = \begin{bmatrix} -\frac{1}{A_1 R_1} & \frac{1}{A_1 R_1} \\ \frac{1}{A_2 R_1} & -\frac{R_1 + R_2}{A_2 R_1 R_2} \end{bmatrix} \begin{bmatrix} h_1 \\ h_2 \end{bmatrix} + \begin{bmatrix} \frac{3}{4A_1} \\ \frac{1}{4A_2} \end{bmatrix} q$$

Descriptor Model

$$\begin{bmatrix} A_1 & 0 & 0 & 0 \\ 0 & A_2 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \dot{h}_1 \\ \dot{h}_2 \\ \dot{q}_1 \\ \dot{q}_2 \end{bmatrix} = \begin{bmatrix} 0 & 0 & -1 & 0 \\ 0 & 0 & 1 & -1 \\ -1 & 1 & R_1 & 0 \\ 0 & -1 & 0 & R_2 \end{bmatrix} \begin{bmatrix} h_1 \\ h_2 \\ q_1 \\ q_2 \end{bmatrix} + \begin{bmatrix} 3/4 \\ 1/4 \\ 0 \\ 0 \end{bmatrix} q$$

Liquid Level Control System - Closed loop

State feedback

$$q = -K_s x_s = -\begin{bmatrix} K_1 & K_2 \end{bmatrix} \begin{bmatrix} h_1 \\ h_2 \end{bmatrix}$$

$$q = -K_d x_d = -\begin{bmatrix} K_1 & K_2 & 0 & 0 \end{bmatrix} \begin{bmatrix} h_1 & h_2 & q_1 & q_2 \end{bmatrix}^T$$

$$\begin{bmatrix} \dot{h}_1 \\ \dot{h}_2 \end{bmatrix} = \begin{bmatrix} -\frac{4 + 3R_1 K_1}{4A_1 R_1} & \frac{4 - 3R_1 K_2}{4A_1 R_1} \\ \frac{4 - K_1}{4A_2 R_1} & -\frac{4R_1 + 4R_2 + K_2}{4A_2 R_1 R_2} \end{bmatrix} \begin{bmatrix} h_1 \\ h_2 \end{bmatrix} \equiv \begin{bmatrix} p_{11} & p_{12} \\ p_{21} & p_{22} \end{bmatrix} x_s$$

$$\begin{bmatrix} A_1 & 0 & 0 & 0 \\ 0 & A_2 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \dot{h}_1 \\ \dot{h}_2 \\ \dot{q}_1 \\ \dot{q}_2 \end{bmatrix} = \begin{bmatrix} -\frac{3}{4} K_1 & -\frac{3}{4} K_2 & -1 & 0 \\ -\frac{1}{4} K_1 & -\frac{1}{4} K_2 & 1 & -1 \\ -1 & 1 & R_1 & 0 \\ 0 & -1 & 0 & R_2 \end{bmatrix} \begin{bmatrix} h_1 \\ h_2 \\ q_1 \\ q_2 \end{bmatrix}$$

The extension of state space results to descriptor systems are not direct.

Example Stability: Classical Result in the Literature

$$\dot{x}(t) = Ax(t) + Bu(t)$$

$$y(t) = Ax(t) + Bu(t)$$

$$A^T P + PA + C^T C = 0$$

Descriptor versions

$$E\dot{x}(t) = Ax(t) + Bu(t)$$

$$y(t) = Ax(t) + Bu(t)$$

$$A^T P E + E^T P A + E^T C^T C E = 0, P \geq 0$$

$$A^T P E + E^T P A + C^T C = 0, E^T P E \geq 0$$

$$A^T (P E + E_0 Q) + (P E + E_0 Q)^T A + C^T C = 0, P \geq 0$$

(Ishihara et al., 2002)

$$A^T X + X A + C^T C = 0, E^T X = X^T E \geq 0$$

Kalman type Filter for Singular Systems

$$E_{i+1}x_{i+1} = F_i x_i + G_i w_i$$

$$z_{i+1} = H_{i+1}x_{i+1} + K_{i+1}v_{i+1}$$

$$\text{cov} \begin{pmatrix} w_i \\ v_{i+1} \end{pmatrix} = \begin{bmatrix} Q_i & S_i \\ S_i^T & R_{i+1} \end{bmatrix}$$

The filtered estimates recursion

$$\begin{bmatrix} \hat{x}_{i+1|i+1} \\ P_{i+1|i+1} \end{bmatrix} = \begin{bmatrix} P_{i|i} & I \\ \begin{bmatrix} Q_i & S_i \\ S_i^T & R_{i+1} \end{bmatrix} & \begin{bmatrix} I \\ I \end{bmatrix} \\ I & \begin{bmatrix} F_i^T \\ \begin{bmatrix} G_i^T & K_{i+1}^T \\ E_{i+1}^T & H_{i+1}^T \end{bmatrix} \end{bmatrix} \end{bmatrix}^{-1} \begin{bmatrix} \hat{x}_{i|i} \\ 0 \\ 0 \\ 0 \\ z_{i+1} \\ 0 \\ 0 \\ -I \end{bmatrix}$$

Kalman type filter for Singular systems

If $S_i = 0, G_i = I, K_i = I$

The filtered estimates recursion

$$\begin{bmatrix} \hat{x}_{i+1|i+1} \\ P_{i+1|i+1} \end{bmatrix} = \begin{bmatrix} P_{ii} & I & 0 \\ \begin{bmatrix} Q_i & S_i \\ S_i^T & R_{i+1} \end{bmatrix} & \begin{bmatrix} I \\ I \end{bmatrix} & \begin{bmatrix} 0 \\ 0 \end{bmatrix} \\ I & \begin{bmatrix} F_i \\ G_i \\ K_{i+1} \end{bmatrix} & \begin{bmatrix} E_{i+1} \\ H_{i+1} \end{bmatrix} \\ \begin{bmatrix} I & 0 \\ I & 0 \\ I & 0 \\ I & 0 \end{bmatrix} & \begin{bmatrix} F_i^T \\ G_i^T \\ K_{i+1}^T \\ E_{i+1}^T & H_{i+1}^T \end{bmatrix} & \begin{bmatrix} \hat{x}_{ii} & 0 \\ 0 \\ 0 \\ z_{i+1} \\ 0 \\ -I \end{bmatrix} \end{bmatrix}$$

Can be rewritten as

$$\hat{x}_{i+1|i+1} = P_{i+1|i+1} E_{i+1}^T \left(Q_i + F_i P_{ii} F_i^T \right)^{-1} F_i \hat{x}_{ii} + P_{i+1|i+1} H_{i+1}^T R_{i+1}^{-1} z_{i+1}$$

$$P_{i+1|i+1} = \left[E_{i+1}^T \left(Q_i + F_i P_{ii} F_i^T \right)^{-1} E_{i+1} + H_{i+1}^T R_{i+1}^{-1} H_{i+1} \right]^{-1}$$

The a priori filter **is not equivalent** to the a posteriori filter

Robust Filtering

- System with uncertainties :

$$(E_{i+1} + \delta E_{i+1})x_{i+1} = (F_i + \delta F_i)x_i + w_i$$
$$z_i = (H_i + \delta H_i)x_i + v_i$$

$$\delta F_i = M_{f,i} \Delta_i N_{f,i}$$

$$\delta E_{i+1} = M_{f,i} \Delta_i N_{e,i+1}$$

$$\delta H_i = M_{h,i} \Delta_i N_{h,i}$$

$$\|\Delta_i\| \leq 1$$

$$\mathbb{E} \left(\begin{bmatrix} x_0 \\ w_i \\ v_i \end{bmatrix} \begin{bmatrix} x_0 \\ w_i \\ v_i \end{bmatrix}^T \right) = \begin{bmatrix} P_0 & & \\ & Q_i \delta_{ij} & \\ & & R_i \delta_{ij} \end{bmatrix} > 0$$

$$\Rightarrow \hat{x}_{k|k}, \hat{x}_{k+1|k}, \hat{x}_{k-1|k}$$

Kalman-type Robust Filter

$$(E_{i+1} + \delta E_{i+1})x_{i+1} = (F_i + \delta F_i)x_i + w_i$$

$$z_i = (H_i + \delta H_i)x_i + v_i$$

Robust filter

$$\hat{x}_{i+1|i+1} = \{P_{i+1|i+1} [\hat{E}_{i+1}^T (\hat{Q}_i + F_i \hat{P}_{i|i} F_i^T)^{-1} F_i + \hat{\lambda}_i N_{e,i+1}^T N_{f,i}] (I - \hat{\lambda}_i \hat{P}_{i|i} N_{e,i+1}^T N_{f,i})\} \hat{x}_{i|i}$$

$$+ P_{i+1|i+1} H_{i+1}^T \hat{R}_{i+1}^{-1} z_{i+1}$$

$$P_{i+1|i+1}^{-1} = \hat{E}_{i+1}^T (\hat{Q}_i + F_i \hat{P}_{i|i} F_i^T)^{-1} \hat{E}_{i+1} + H_{i+1}^T \hat{R}_{i+1}^{-1} H_{i+1}$$

$$+ \hat{\lambda}_i [N_{h,i+1}^T N_{h,i+1} + N_{e,i+1}^T (I + \hat{\lambda}_i N_{f,i} \hat{P}_{i|i} N_{f,i}^T)^{-1} N_{e,i+1}]$$

Future work related to PROBRAL

1) Descriptor systems with Markovian jumping

$$E_{\theta(i+1)}x_{i+1} = F_{\theta(i)}x_i + G_{\theta(i)}w_i$$

$$z_i = H_{\theta(i)}x_i + K_{\theta(i)}v_i$$

Already done: array algorithms for filters of Markovian jumping Linear systems

2) other possibilities?

Conclusion & Perspectives

- Wire Less Automated Building as NCS Test Bed
- Modelling of Thermal Processes
- Stability Analysis of NCS + Distributed Automation
- Specific Hardware x COTS for distributed automation

? UnB + KL ?

Danke! Obrigado!

Wir freuen uns auf die Zusammenarbeit!

adolfo@unb.br
www.lavsi.ene.unb.br
www.ene.unb.br/adolfo

