Computational fluid dynamics simulations guided by Fourier velocity encoded MRI

Vinicius Rispoli¹, Jon-Fredrik Nielsen², Krishna Nayak³, and Joao Luiz Carvalho¹

¹University of Brasilia, Brasilia, DF, Brazil, ²University of Michigan, Ann Arbor, MI, United States, ³University of Southern California, Los Angeles, CA, United States

Introduction: Fourier velocity encoding $(FVE)^{[1]}$ is a promising MRI method for assessment of cardiovascular blood flow. FVE provides considerably higher signal-to-noise ratio (SNR) than phase contrast (PC) imaging, and is robust to partial-volume effects. On the other hand, FVE does not directly provide velocity maps. These maps are useful for calculating the blood flow through a vessel, or for guiding computational fluid dynamics (CFD) simulations^[2,3]. PC-driven CFD has been previously demonstrated^[2,3], and can be useful for reducing scan time, improving spatial resolution, and/or denoising the MRI data. This work introduces a method for using FVE data (rather than PC data) to guide CFD simulations.

Methods: Simulated FVE data was derived from 3DFT FGRE PC data from a pulsatile carotid flow phantom (Phantoms by Design, Inc., Bothell, WA). PC imaging was performed on a 3T GE Discovery MR750 system (50 mT/m, 200 T/m/s), using a 32-channel head coil. Scan parameters: resolution = $0.5 \times 0.5 \times 1.0$ mm³; FOV = $16 \times 12 \times 7.5$ cm³; Venc = 50 cm/s; TR = 11.4 ms; flip angle = 8.5° ; temporal resolution = 91.2 ms; scan time = 40 minutes; 9 NEX; pulse cycle 60 bpm). The spin-density map (magnitude image), m(x,y), and the through-plane velocity map, $w_{pc}(x, y)$, corresponding to a temporal frame at mid-systole, were used to simulate a spiral FVE^[4] spatial-velocity distribution, according to the signal model^[5]: $s(x, y, w) = \left[m(x, y) \cdot \operatorname{sinc}\left(\frac{w - w_{pc}(x, y)}{\delta w}\right)\right] * \operatorname{jinc}\left(\frac{\sqrt{x^2 + y^2}}{\delta r}\right)$, where x and y are the in-plane spatial coordinates, w is the through-plane velocity, and δr and δw are FVE's spatial and velocity resolutions, respectively. The spatial blurring effects of the jinc kernel were reduced using a deconvolution algorithm^[6] to obtain $\tilde{s}(x, y, w)$. Then, an estimate of the true velocity at a given spatial coordinate (x_o, y_o) was estimated from $\tilde{s}(x, y, w)$ as^[7]: $\hat{w}(x_o, y_o) = \arg\min_{\mu} \left\| \frac{\hat{s}(x_o, y_o, w)}{m(x_o, y_o)} - \operatorname{sinc}\left(\frac{w - \mu}{\delta w}\right) \right\|_2$. Finally, CFD

calculations were performed using a modified version of the SIMPLER algorithm^[2,3], in which $\hat{w}(x, y)$ was used to constrain the CFD calculation. The phantom's bloodmimicking fluid (viscosity 5 mPa.s, density 1100 kg/m³) was assumed to be Newtonian, isothermal, and incompressible. The simulation grid was designed with $0.5 \times 0.5 \times 1.0$ mm³ resolution, and a computational time step $\delta t = 0.25$ ms was used. Finally, the estimated flow field was compared quantitatively and qualitatively with both a pure CFD solution and the PC-measured flow field. This process was repeated for different values of δr (1 or 2 mm); and for each slice along the *z* axis. The velocity resolution, δw , was 10 cm/s.

Results and Discussion: The spin-density maps in Fig. 1a illustrate the spatial blurring associated with each value of δr , for a slice perpendicular to the phantom's bifurcation. Fig. 1b presents the FVE-estimated velocity maps, \hat{w} , for each spatial resolution value, while Fig. 1c shows the associated errors (relative to the PC map, w_{pc}). The results show that lower error levels were obtained when FVE data with finer spatial resolution was used. In this slice, the absolute error was greater than 5 cm/s for only 10% of the voxels when $\delta r = 1$ mm was used; while 31% of the voxels presented error greater than 5 cm/s when $\delta r = 2$ mm was used. Fig. 2 shows (i) the PC-measured velocity field; and the CFDsimulated velocity fields, obtained using (ii) pure CFD, (iii) FVE-driven CFD ($\delta r = 1$ mm), and (iv) FVE-driven CFD ($\delta r = 2$ mm). Considerable qualitative improvement with respect to agreement with the PC reference — can be appreciated in the FVE-driven results, when compared with the pure CFD result. Table 1 presents the measured signal-toerror ratio (SER) relative to the PC reference, for the CFD results shown in Fig. 2. Both FVE-driven solutions achieved higher SER than the pure CFD approach, when evaluating the three-dimensional velocity vector $\vec{v} = (u, v, w)$; the SER gain (relative to pure CFD) was 1.49 dB when $\delta r = 1$ mm was used, and 0.80 dB when $\delta r = 2$ mm was used. When evaluating only the y-axis velocity component (v), there was a 0.11-0.35 dB loss in SER with the proposed method. This may be a positive effect of denoising, since the velocities along that axis are extremely low (v_{pc} 's total energy is 15.7 dB lower than that of w_{pc}). Nevertheless, the SER gains for the *u* and *w* components more than compensate for this. *Conclusion*: This work presented a method for using FVE data to guide CFD simulations. We showed that FVE-driven CFD achieves better agreement with a PC-measured velocity map than pure CFD solutions. This is an important result, since a 1-mm resolution spiral FVE dataset could be acquired in the same scan time as 1 NEX of a 0.5-mm resolution PC dataset with the above parameters; however the FVE dataset would have an SNR 23 dB higher than that of PC (for a 2-mm resolution spiral FVE, scan time would be 3 times

shorter, and the SNR would still be 8 dB higher than those of PC). **References:** [1] Moran PR. MRI 1:197. [2] Nielsen JF et al. Proc ISMRM 17:3858, 2009. [3] Rispoli VC et al. Proc ISMRM 22:2490, 2014. [4] Carvalho JLA and Nayak KS. MRM 57:639, 2007. [5] Carvalho JLA, et al. MRM 63:1537, 2010. [6] Krishnan D and Fergus R. Proc 24th NIPS, 2009. [7] Rispoli VC and Carvalho JLA. Proc ISMRM 21:68, 2013.



Figure 1: (a) Spin-density maps for PC (0.5 mm spatial resolution), FVE with 1 mm spatial resolution, and FVE with 2 mm spatial resolution, for a slice perpendicular to a carotid phantom's bifurcation; (b) corresponding velocity maps; and (c) absolute error for the FVE-estimated velocity maps, relative to the PC reference.



Figure 2: 3D visualization of the velocity fields, comparing the PC reference with each CFD approach.

Table 1: SER between each of the CFD approaches and the PC reference.			
	Pure CFD	CFD + FVE	CFD + FVE
		$\delta r = 1 \text{ mm}$	$\delta r = 2 \text{ mm}$
SER_u	2.97 dB	3.93 dB (↑)	3.81 dB (†)
SER_{v}	-0.25 dB	-0.36 dB (↓)	-0.60 dB (↓)
SER_w	5.44 dB	10.97 dB (†)	7.22 dB (↑)
$SER_{\vec{v}}$	6.57 dB	8.06 dB (↑)	7.37 dB (↑)

Table 1. CED hater